

Bonnell & Lundahl

Experiments
With Fan Blowers

Mech. Engineering

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EXPERIMENTS WITH FAN BLOWERS

BY

EVERETT SHANNON BONNELL

AND

BRUCE HJALMAR LUNDAHL

THESIS FOR THE DEGREE OF BACHELOR OF SCIENCE
IN MECHANICAL ENGINEERING

IN THE
COLLEGE OF ENGINEERING
OF THE
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190

THIS IS TO CERTIFY THAT THE THESIS PREPARED UNDER MY SUPERVISION BY

EVERETT SHANNON BONNELL and BRUCE HJALMAR LUNDAHL

ENTITLED EXPERIMENTS WITH FAN BLOWERS

IS APPROVED BY ME AS FULFILLING THIS PART OF THE REQUIREMENTS FOR THE DEGREE

OF Bachelor of Science in Mechanical Engineering

L. P. Brickmeyer

HEAD OF DEPARTMENT OF Mechanical Engineering

Introduction.

The ordinary centrifugal fan or exhauster consists of a number of blades fixed to arms, revolving on a shaft at high speed. These blades usually are inclosed in a casing which is always of a spiral form. They are adapted to the movement of large volumes of air at pressures varying from one to twenty ounces. With a fan the air is generally discharged into the atmosphere, while with the exhauster it is drawn from the atmosphere.

Classification.—The classification of centrifugal fans is as follows:

Steel Pressure Blowers.

Volume Blowers.

Volume Exhausters.

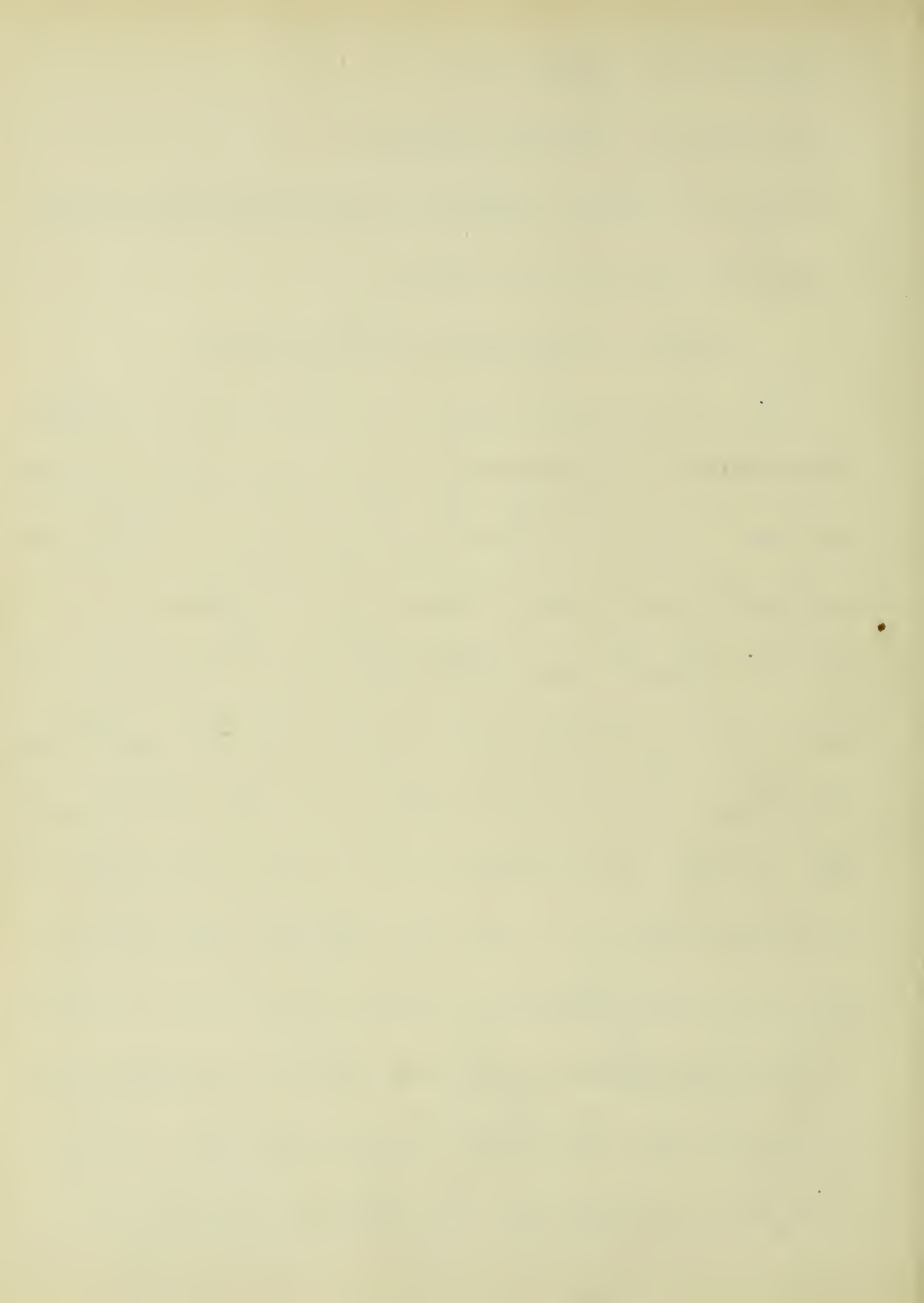
Steel Plate Blowers, and Exhausters.

Sirocco Blowers.

Steel Pressure Blowers.

The steel pressure blower is a fan designed to deliver a small volume of air at a high pressure. They are capable of producing a pressure of as high as twenty ounces, and are adapted for use with cupolas, forges and mechanical stokers.

In order to obtain a small volume of discharge at a high pressure, pressure blowers are made with blast wheels of small widths as compared to their diameters. The blades, varying in number from



-Five to eight, are wider at their inner ends than at their outer circumference, where they are curved backward to allow the air to easily leave the wheel, and to diminish the noise of the fan when running at a high rate of speed. The Sturtevant pressure blowers are built with six blades and twelve or eighteen smaller ones. These small blades are of about half the length as the large ones, between which they are placed. The large blades are all riveted to "T" irons cast on the hub of the blast wheel, while the small blades are riveted to and carried by the conical side plates which ^{extend} from the inlet to the outer

circumference of the wheel. The ^{5.}side ^{plates},
in turn are carried by the large
blades of the wheel. The casing,
always of a spiral form, is made
of cast iron and usually has its
discharge opening horizontal and
at the bottom. The shaft is of steel
and is hung in two large self-
oil-lubricating bearings, generally of the ring and
wick type. A bearing is placed on
each side of the fan casing and
supported by a pedestal which is
either cast on the casing or bolted
to it. Both one and two driving
pulleys are used. Pressure Blowers
are always mounted on an ad-
justable bed plate but are never directly
connected to the engine, as the

relative speed is too high.

Volume Blowers.

This type of blower is designed and built to discharge a large volume of air against a moderate pressure, two to ten ounces per square inch. In appearance they are very similar to the pressure blowers. The casing, however, is wider and the outlet larger in proportion than in the former. The fan blades in some cases are of an equal width the whole length and are also bent backward as in the pressure blowers. Only one driving pulley is used. Volume blowers also are mounted on adjustable bed plates, and if the relative speed is not to

high may be directly connected to the engine.

Volume Exhausters.

The construction of the general type of volume exhausters is not unlike that of the volume blower, except that there is only one inlet and that the shaft is overhung in two bearings, both of which are placed on the opposite side of the casing from the inlet. The bearings have the driving pulley placed between them and are supported by pedestals in the same manner as in the blower.

Steel Plate Blowers and Exhausters.

This line of blowers and exhausters is built to handle large

volume of air at very low pressures, such as are wanted for ventilating purposes, where this type of fan finds a large field of application. The casing is of steel plate riveted to angle irons for stiffening. There are, as a rule, eight to twelve blades on the blast wheel, which are supported and carried by two or more cast iron spiders. The number of the latter depending upon the size of the fan. The blades are always made straight, seldom if ever being curved backward and then only very slightly right at the tip. The discharge opening may be placed in any

position or direction which is at right angles to the plane of the shaft of the machine. The casing being built in such a manner that it may be revolved around the shaft and fastened at any desired point. A great many of the larger sizes of steel plate blowers and exhausters are fitted with two discharge openings and are run by a direct connected engine.

The Sirocco Blower.

This is a type of fan used very extensively in mining, where it seems to give excellent results. The chief points of its construction are as follows:— The blades

are very numerous, with their radial measurements (relative to the diameter of the fan) very shallow, and their axial measurements very long. Their outer edges are curved forward in the direction of rotation, and the air passages between the blades are usually open at the ends toward the inflowing air. The inlet for admitting air to the fan, and the outlet for its discharge, are approximately of equal diameter to the fan itself. All of these features constitute practically a reversal of previous theory and practice in regard to fan construction, never

the less, it is claimed that the actual effect of this design is to materially increase the volume of air discharged per revolution. The sirocco fan is well adapted to high speed and therefore to electric driving.

Experiments.

The following series of experiments on Centrifugal Fans and Exhausters was conducted by the writers in the Mechanical Engineering Laboratory of the University of Illinois.

Object.

The object of the tests made on the fans and exhausters was the determination of their

capacity to move a given volume of air under conditions with respect to the pressure and size of opening of the discharge pipe. Also the determination of the power required for moving a given quantity of air under the conditions named above, and finally, the efficiencies of the fans and exhausters. From the complete tests, as outlined, were determined the most economical conditions under which certain quantities of air could be moved. In order to meet these requirements it was necessary to make accurate measurements of: first, the power required to operate the fan; second,

the volume of air delivered by the fan; third, the pressure produced and fourth, the power required.

Referring to these several requirements, the object may be briefly stated as follows, for each condition.

1. How the quantity of air discharged varies with the speed.
2. How the pressure varies with the speed.
3. How the horse power varies with the speed.

Apparatus.

The arrangement of the apparatus whereby the actual measurements of the horse-power, volume of air discharged, compression and speeds were obtained in each

experiment is shown by plates I. and II. pages 21 and 22 respectively. The fans and exhauster were driven from a counter shaft, which derived its motion from a twenty five horse-power, horizontal Ball Engine. ^(See page 20) The outlet of the fans and the intake of the exhauster was fitted with a circular galvanized iron pipe twelve feet long, the diameter of which was such as to just fit the opening. A sliding gate (See fig. 2 Plate I.) was attached to the end of the circular pipe, and by means of it the discharge opening of the fan and intake of the exhauster was varied to suit the different conditions under which

the experiment was run. A Crosby Steam Indicator was used to find the indicated horse-power. In all the experiments hand speed counters were used to obtain the R.P.M. of the engine. For obtaining the speeds of the fans and exhauster a calibrated tachometer was used when the arrangement of the fan shaft was such as to permit the tachometer belt to be run upon it, otherwise the speed was obtained with a hand speed counter.

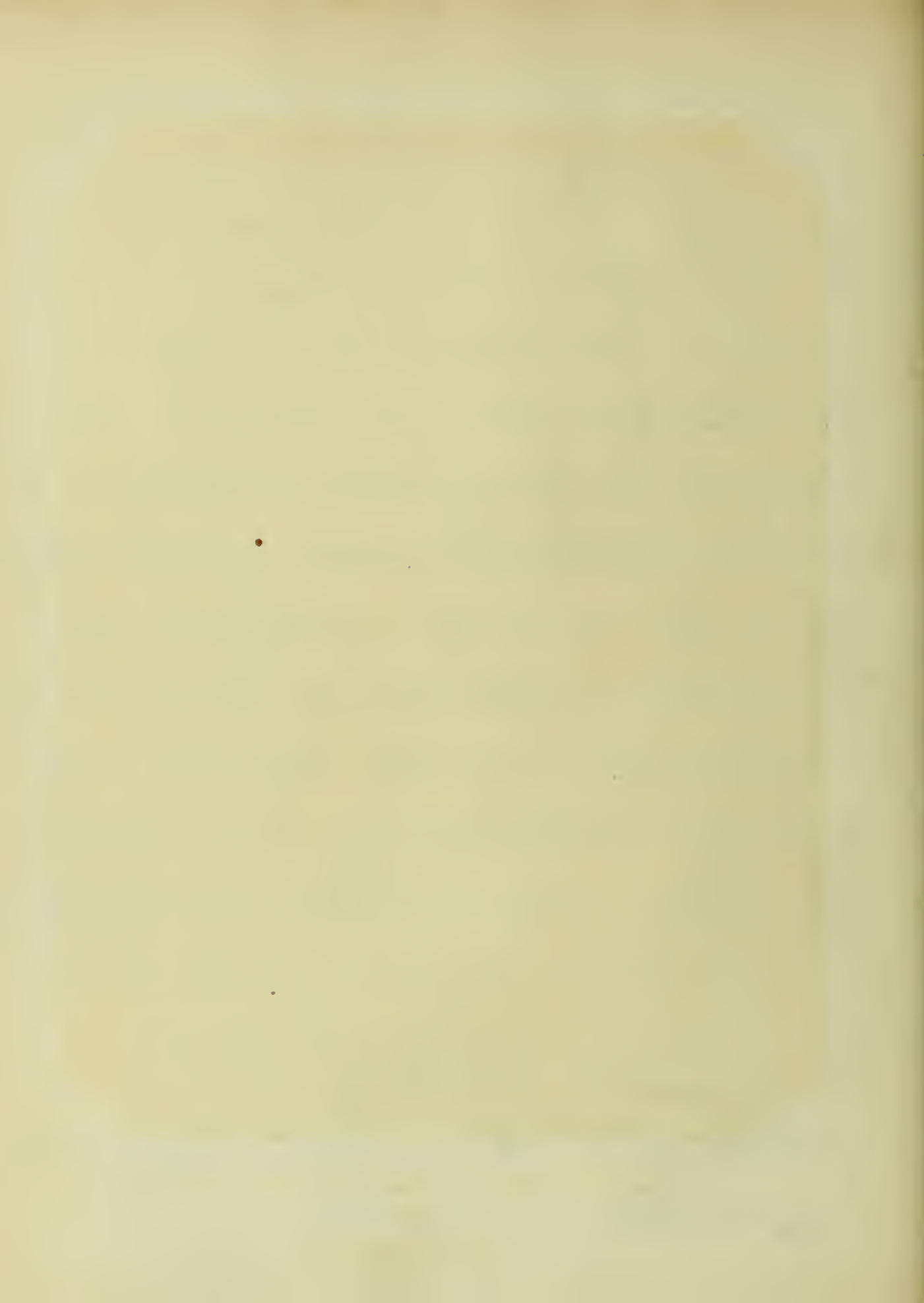
Measurements of the pressure and velocity of the air stream were taken at a section of the pipe five feet from the discharge opening of the fan and seven

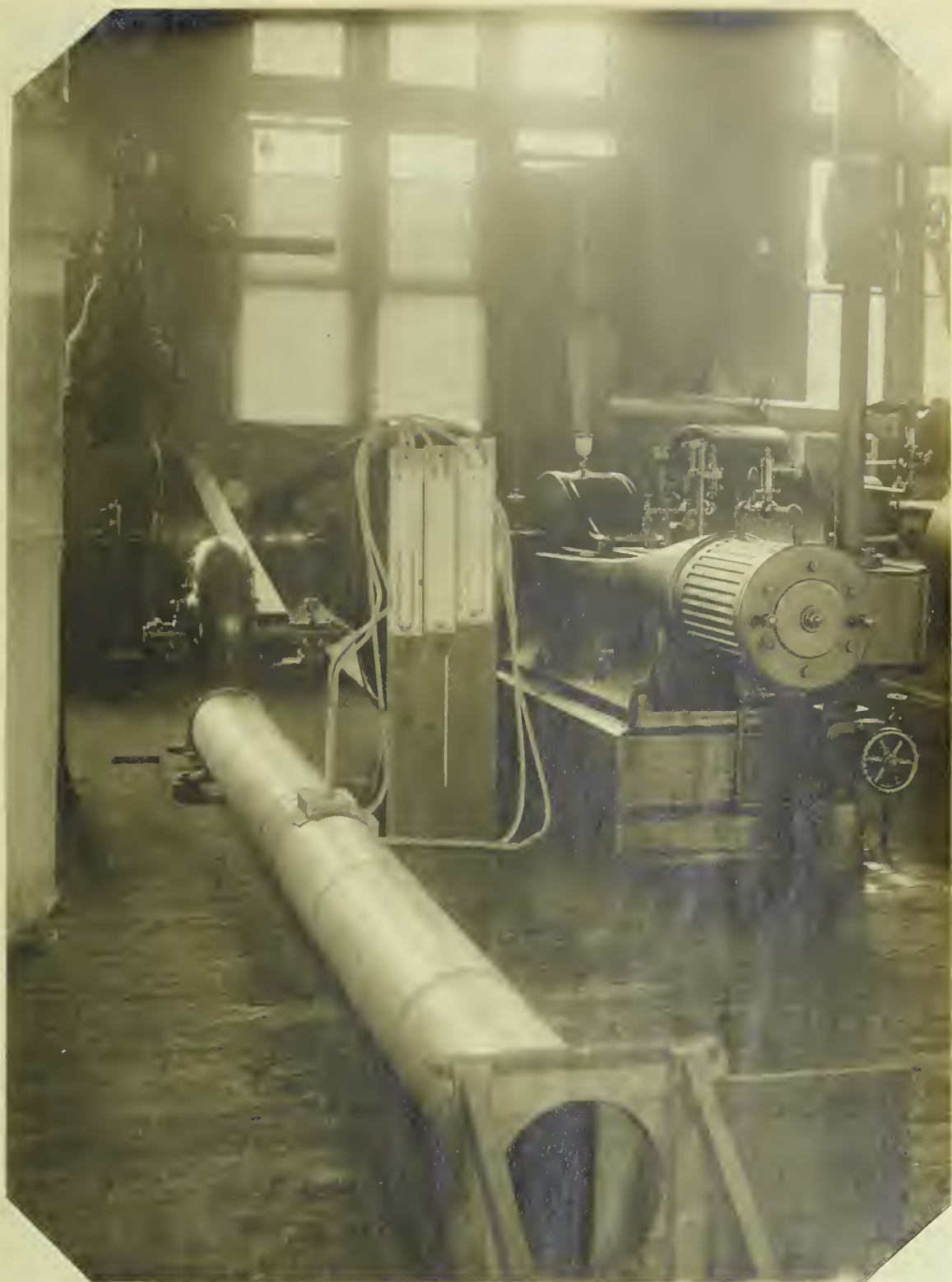
seven feet from the intake opening of the exhauster. The pressure of the air was measured with a U shaped gage made from $\frac{1}{4}$ inch glass tubing, and of such a length as would permit the registration of 14" of water. One arm of the gage was open to the atmosphere, while the other was connected by means of rubber tubing to a small pipe, or tip, soldered on to ^{the} side of the delivery tube. The scale used for reading the height of the water column was ruled in ounces and tenths of ounces. For measuring the velocity of the air a combination of the Pitot tube and the pressure gage

was resorted to. Readings were taken at several points in the cross-section of the pipe by means of two velocity tips, each of which could be traversed over a diameter at right angles to the other. The water gage was of a similar type and construction as was used for the pressure readings, with the exception that its scale was ruled in inches instead of ounces. The velocity tips used (See fig. 5 Plate II, page 22.) consisted of a Pitot tube and a straight tube, having a small circular guide, or side tip, glued on to the end of it. These two tubes were wired together and clamped onto a thin flat stick to give them sufficient strength. The purpose

of the guide was to eliminate the error that presents itself in the measurement of compression, owing to the fact that air flowing across the end of a plain tube causes a large amount of induction; a vacuum being often recorded when a pressure is known to exist. One of the branches, of the U tube, of the velocity gage was connected to the Pitot tube by means of rubber tubing and the other to the tube of the side gage. (See figures 1, 2 and 3 Plate II page 22.) The pressure in the arm connected to the straight tube, or side tip, will be due to the ^{pressure} ~~conc.~~ of the air only, while the pressure in the arm connected with the

Pitot tube will be due to pressure and velocity combined. Hence the reading of the water gage will be the difference of these pressures, which is that due to velocity alone. The velocity tips were held in position by inserting them through suitable openings cut in small boxes which were firmly wired over the holes cut in the delivery tube for inserting the velocity tips. The Pitot tube was placed so that it always faced the current. The U tubes and velocity tips were all made from $\frac{1}{4}$ inch glass tubing, the small circular guides, or side tips, were made of oak, their dimensions being given in fig. 4, Plate II. page 22.





GENERAL ARRANGEMENT
OF
APPARATUS

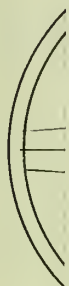
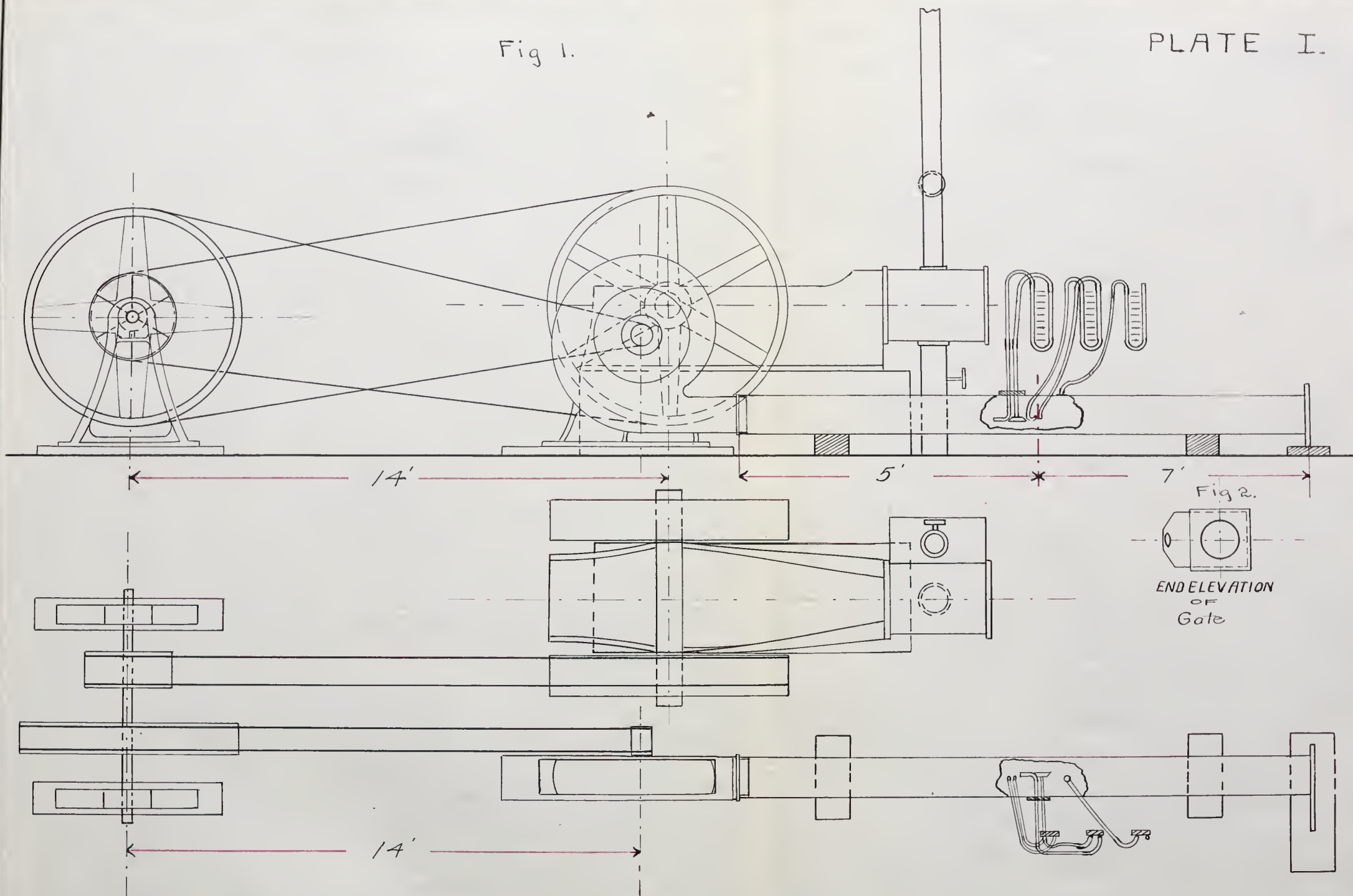


Fig 1.



FAN-TESTING APPARATUS.

المسألة الأولى

المسألة الثانية



PLATE II.

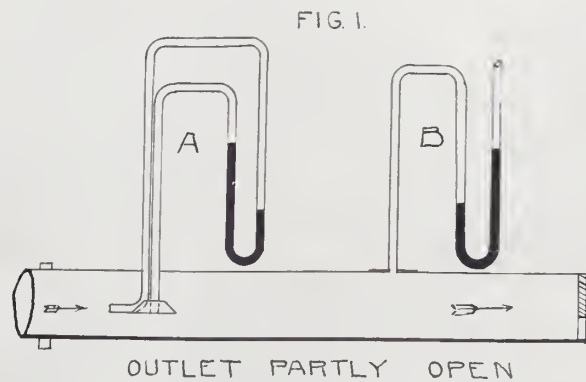


FIG. 4.
VELOCITY TIP
SCALE $1/4" = 1"$

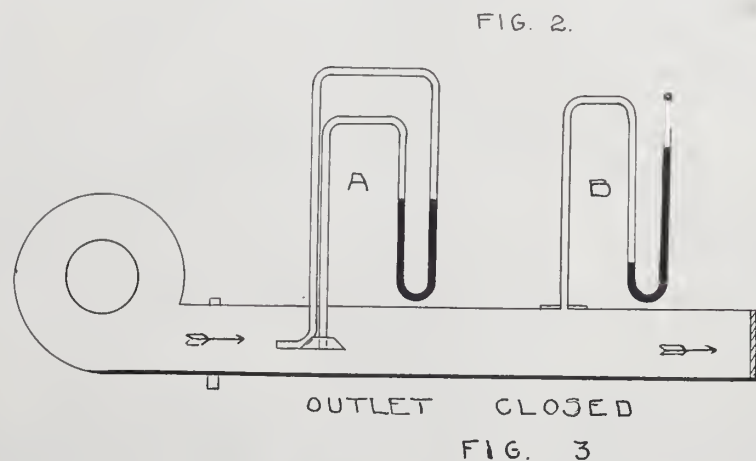
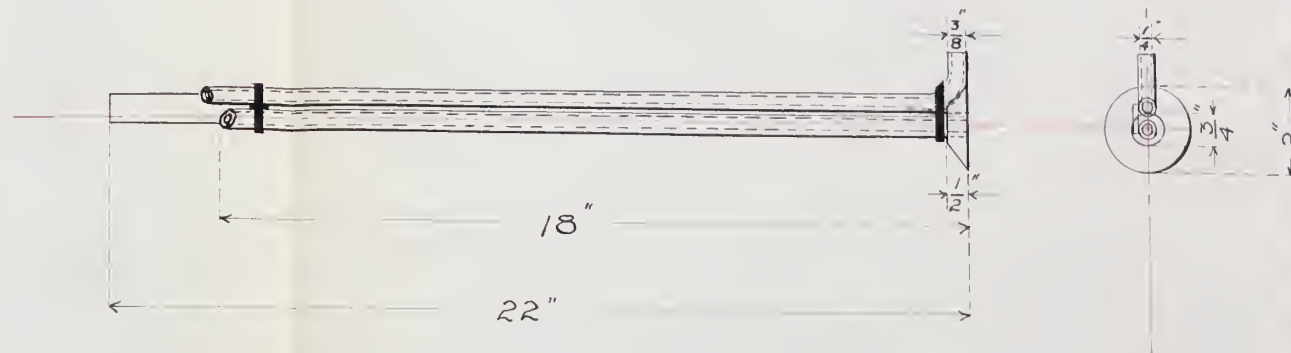
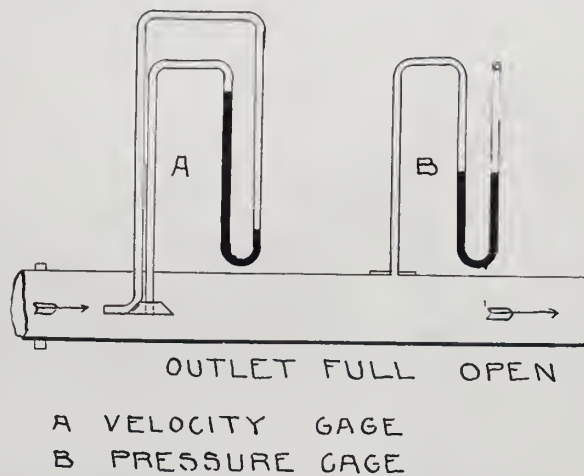
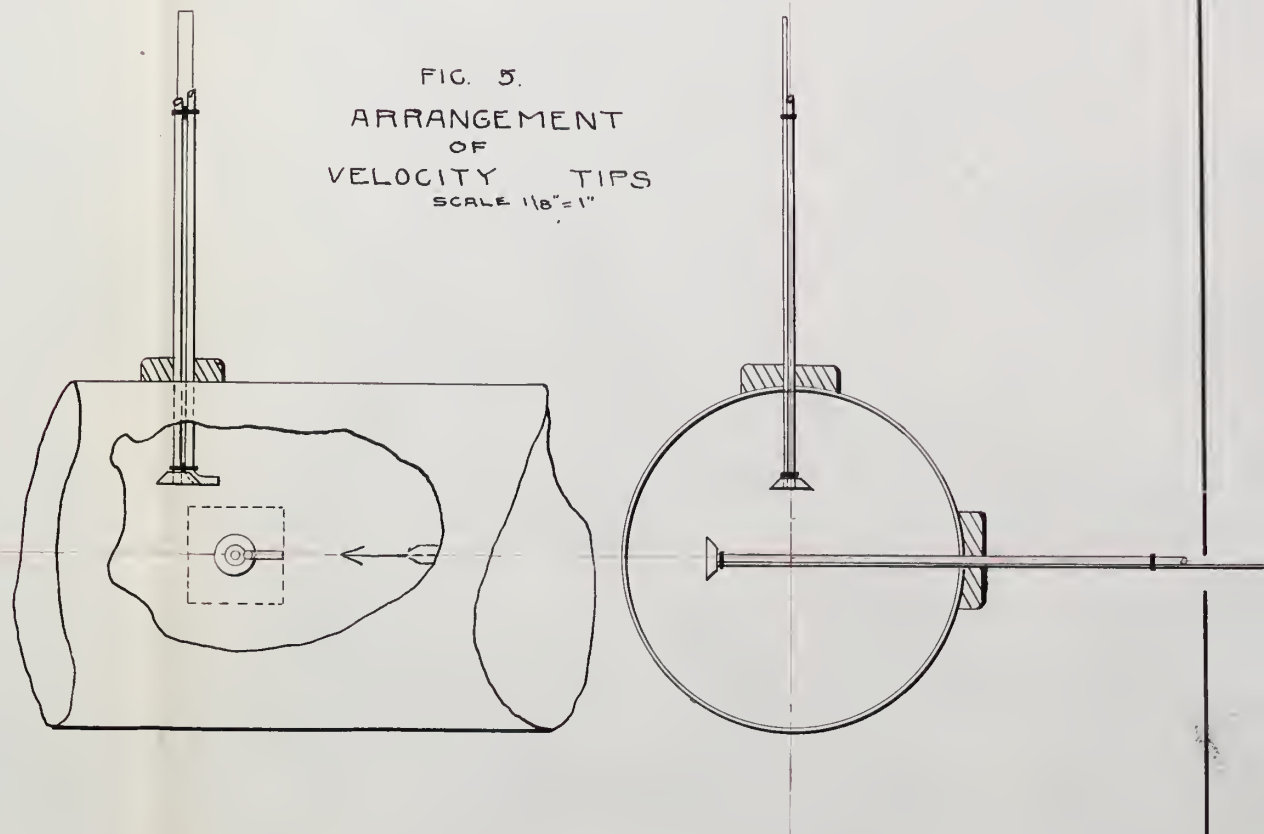


FIG. 5.
ARRANGEMENT
OF
VELOCITY TIPS
SCALE $1/8" = 1"$



APPARATUS FOR MEASURING
PRESSURE AND VELOCITY

Method.

General Outline of Tests: In each set of experiments the quantity of air passed was varied, thus producing a corresponding change in the pressure and power required to drive the fan. This was easily and quickly effected by throttling the flow of air in the delivery tube by means of an air gate placed at the end of the tube. In each experiment, for every speed run, the air was made to pass through this gate successively at full, $\frac{1}{4}$, $\frac{1}{2}$, $\frac{3}{4}$ and zero ^{gate} opening, except in the case of the No. 1. Sturtevant Blower. Its delivery tube being so small that full $\frac{1}{3}$, $\frac{2}{3}$ and zero gate openings were used.

From eight to twelve speeds were run for each gate opening, they lying between those for which the fan was designed to run.

Speed.- The governor of the engine used to drive the fan was blocked out and the different speeds were obtained by means of a throttling valve placed in the steam-pipe.

Horse-power.- A Crosby Steam Indicator was used for taking indicator cards by means of which the I. H. P. was determined. A friction test was run on the engine and counter shaft and a friction curve was plotted for the various speeds; by the use of it the H. P.

consumed by the engine and counter shaft could be found for any speed. Subtracting this result from the A.H.P., at the same speed, gave the actual H.P. consumed by the fan alone.

Order of taking readings. - Corresponding to the various speeds, readings were taken for gate openings in the following order: full, $\frac{1}{4}$, $\frac{1}{2}$, $\frac{3}{4}$ and zero. The gate was first set at full opening and the speed of the fan brought up to the desired point, where it was run for a short time to assure its remaining constant, then the R.P.M. of the fan and engine were taken simultaneously, after which, one

man took the indicator card, while the other read the pressure and velocity gages as quickly as possible: these readings were checked by reading the gages twice. The remaining gate openings were then taken in the order named. The velocity gages were marked at points corresponding to the distances to which they would have to be inserted into the delivery tube, to correspond to the centers of the equal areas into which the cross section of the tube was supposed to be divided, in order that they might be the more quickly manipulated and read. The horizontal ^{velocity} gage was always read first

then the vertical velocity gage after which the pressure was noted.

Temperature and Barometer reading. - The average temperature was determined by placing a thermometer at the discharge opening and taking a reading every thirty minutes. The barometer readings recorded are the averages for the days on which the tests were run.

Calculations.

Actual Horse-power to Drive the Fan. - The measurement of the total horse-power required to operate the fan was obtained from indicator diagrams taken as previously explained. This indicated horse power, however, shows not the power applied to the fan,



but the power applied to the piston of the engine. To find the actual H.P. used to drive the fan, this I. H.P. was decreased by the amount of the power absorbed by the friction of the engine and counter shaft. A friction test was run on the engine and counter shaft at a wide range of speeds and the results plotted. From the curve thus obtained could be determined the friction H.P. for any speed. Subtracting this result from the I. H.P. taken at the same speed the actual H.P. to drive the fan was obtained.

Pressure.— The pressure was read directly from the gage in ounces,

(see description of pressure gage, page)
 thus eliminating the calculation of
 each pressure separately, if the read-
 ings had been taken in inches of
 water. The calculation for reducing
 inches of water to ounces of pressure,
 in order to rule the scale in ounces
 was made as follows:—

1 lb. press. corresponds to 2.304 ft. of water.

16 oz " " " " 27.648 in. " "

1 oz " " " " 1.727 " " "

This length in inches (1.727") correspond-
 ing to one ounce of pressure was
 subdivided into tenths and the
 scale ruled accordingly.

Velocity.— The calculation of the
 velocity was made according to
 the formula deduced by Homan

and Gilbert. in Vol. 123, of the P. L. C. E.. Suppose the air to be flowing directly against the mouth of a tube which is connected to a gage for the purpose of measuring the pressure produced by this velocity. The pressure h , in feet of air due to a velocity of v ft. pr. sec. is $h = \frac{v^2}{2g}$ (1).

If h be measured in inches of water, as it would be measured in practice, regard must be had to the relative densities of air and water at the time of the experiment.

Let h = pressure measured as a column of air in feet.

Let i = the corresponding pressure measured in inches of water.

T = the absolute temperature of the air in degrees Fah.

h_0 = height of the barometer in inches of mercury.

Then PV being equal to $53.2 T$ for one pound of air, when P , the pressure of the atmosphere, would be measured by a barometer, the following numerical relation is found between h and i' :-

$$h = 3.91 \frac{i' \times T}{h_0} \quad (2).$$

H.P. of fan = $\frac{V \times i}{6.352}$ (3). This equation is deduced under the heading of theoretical horse-power.

Substituting the value h in equation

$$(3) \quad i' = \frac{V^2 h_0}{251.7 T} \quad (4)$$

This formula gives the reading of the water-gage due to velocity V .

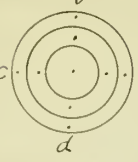
for any given atmospheric condition of barometer and temperature.

When $T = 60^{\circ}\text{F}$ and $h_v = 30''$ mercury

$$i' = \frac{V^2}{4370} \text{ or } V = \sqrt{i' \times 4370}.$$

In applying this formula to obtain our results the average values of the temperature, barometer and i' readings were used.

Volume.— The volume of air delivered was found by obtaining the average velocity of the air in the discharge pipe and multiplying it by the area in sq. ft. of the pipe. This average velocity was obtained as follows:— the discharge pipe, in each case, was divided into a number of equal areas and four readings

taken in each area (as at a, b, c and d ). The mean of these readings was taken as the velocity of that area. The velocities of the remaining areas were found in the same manner and then the average of the velocities of all the areas was taken as the correct velocity of the air in the delivery tube. With the average velocity known the volume in cu. ft. per sec. was computed by multiplying the velocity in ft. per sec. by ^{of a cross section} the area of the discharge pipe in sq. ft. The amount of air discharged per H.P. per sec. was obtained by dividing the discharge in cu. ft. per sec. by the H.P.

required to drive the fan at that velocity.

Theoretical Horse power:— The work done by the fan in ft. lbs. per lb. of air entering the fan is.—
Volume of air in cu. ft. per lb. \times the increase in pressure in lbs. per sq. foot, and where,

V = Vol. of air entering fan in cu. ft. p. min.

i = Press. in inches of water. A

pressure of 1 inch of water being equivalent to 5.2 lbs. pr. sq. ft.

$$\text{Theoretical H.P.} = \frac{V \times 5.2 i}{33000} = \frac{V \times i}{6352}.$$

Since 1 ounce of pressure = 9 lbs pr. sq. ft. the above formula reduces to the form,

$$\text{Theoretical H.P.} = \frac{V \times 0.7}{3666.66}.$$

Efficiency:— The efficiencies of

the fans and exhauster was found
by dividing the theoretical H.P. by
the actual H.P. required to drive
the fans.

EXPERIMENT NO. 1

Buffalo Volume Blower No. 8.

See Plate II. ^{p. 40.} The general structural details of this blower are as follows: To the solid (cast iron) outer peripheral shell, which carries likewise the discharge orifice, are securely bolted two side plates, in which are formed the inlets. The pedestals carrying the standard oil ring bearings are bolted to these side plates. The blower is built with only one driving pulley. Its blast wheel is built with five wrought iron, radial spokes, bent backward at their outer ends, each carrying a blade which continues this backward curvature of the spokes to

to their outer circumferences. Thus making a total backward curvature of 3 inches. Conical side plates are riveted to the spokes and extend entirely around the wheel thus making it very rigid.

Table of Dimensions:-

Height Total	48"
Length " "	47.5"
Width " "	40."
Diam. of Pulley	8.5"
Width " "	7.5"
Diam. of Blast Wheel	28"
Width " " " "	11"
No of Blades	5
Size " " "	11" x 9"
Area of " "	88 sq.in.
Waim. Outlet (outside of flange)	16.5"

diam. of Outlet (inside of pipe flange)	13"
Area " " "	132.7 sq. in.
diam. of Inlet. (pulley side)	13.5"
Area " " " " "	86.4 sq. in.
The area of the pulley was subtracted as it obstructed the opening.	
diam. of Inlet. (opposite side)	13.5"
Area " " "	114 sq. in.
Ratio $\frac{\text{Area of Inlet}}{\text{Area of Outlet}} =$	1.56
diam. of Shaft.	1.75"
Length of Bearings	9"

Temperature and Barometer Readings.

Barometer (average)	29.7"
Temperature	80.8°F

PLATE III.
BUFFALO VOLUME BLOWER NO 8.

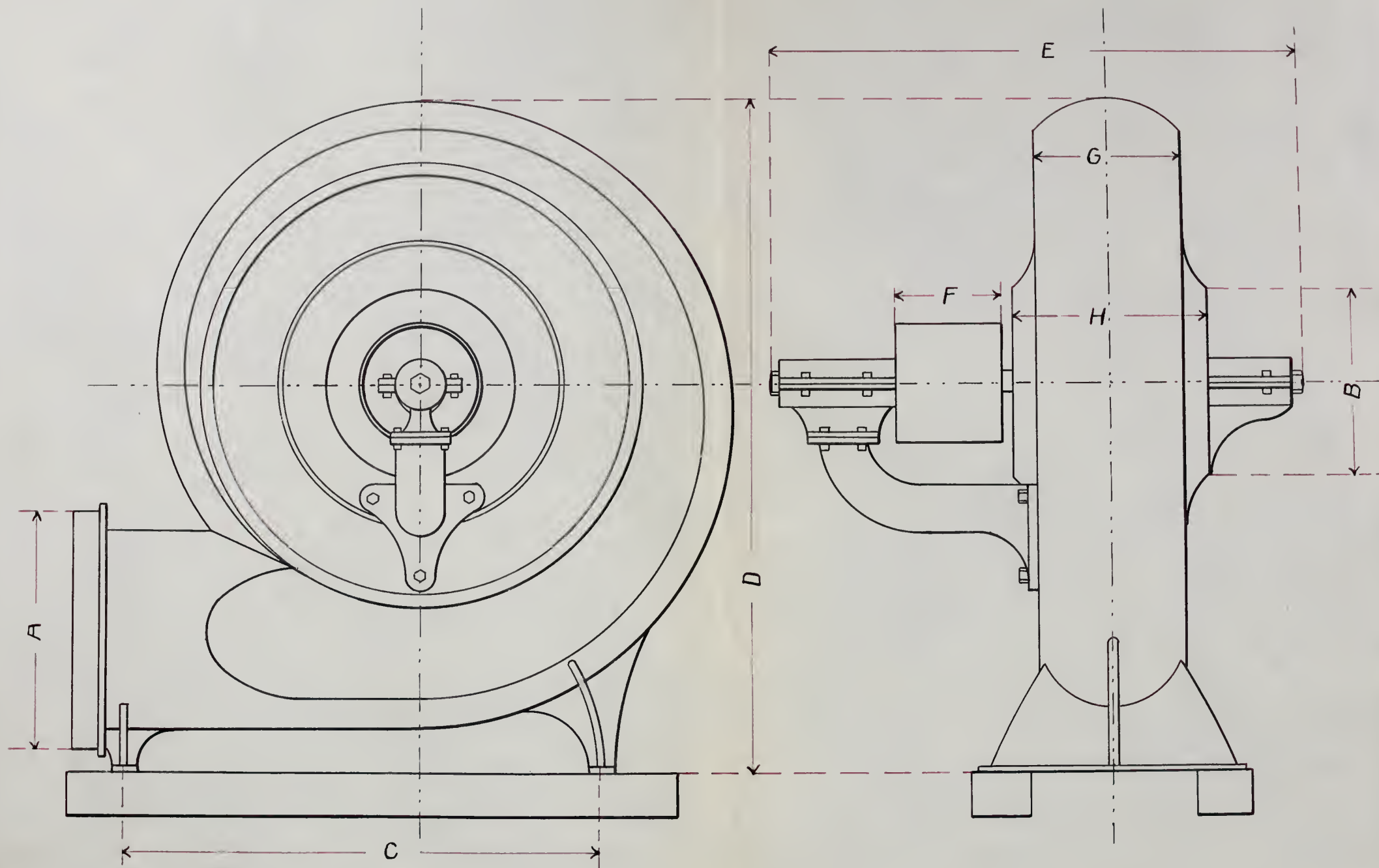


TABLE 1.

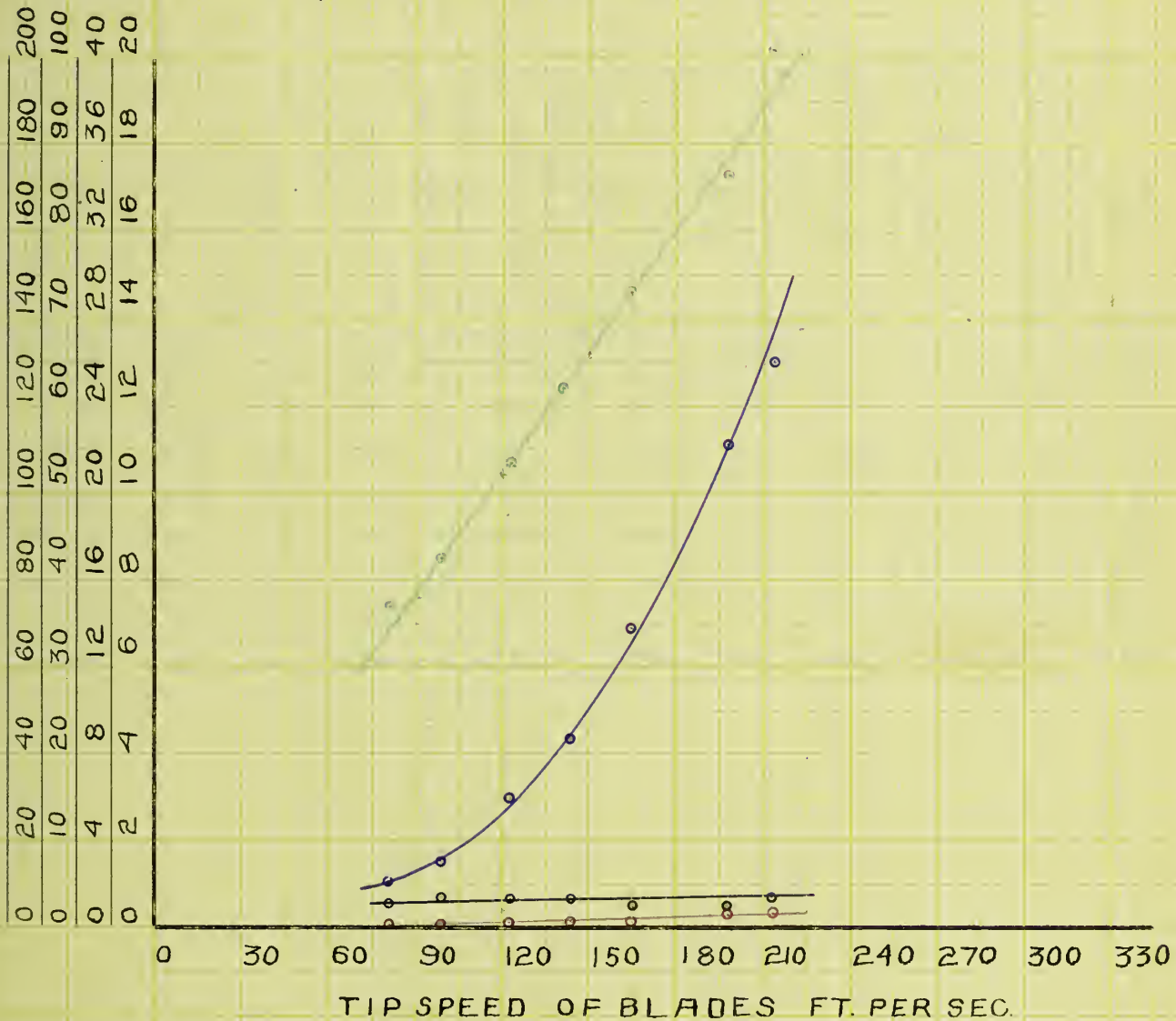
DATA AND RESULTS
FOR
BUFFALO BLOWER NO 8.
FULL OPENING
OF
DISCHARGE

[illegible]

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE I.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

VOLUME
EFFICIENCY
H. P.
PRESSURE



1875

TABLE 2.

DATA AND RESULTS
FOR
BUFFALO BLOWER NO 8.

$\frac{3}{4}$ OPENING
OF
DISCHARGE

[illegible]

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 2.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

200
100
40
20
180
90
36
18
160
80
32
16
140
70
28
14
120
60
24
12
100
50
20
10
80
40
16
8
60
30
12
6
40
20
8
4
20
4
2
0

VOLUME
EFFICIENCY
H.P.
PRESSURE

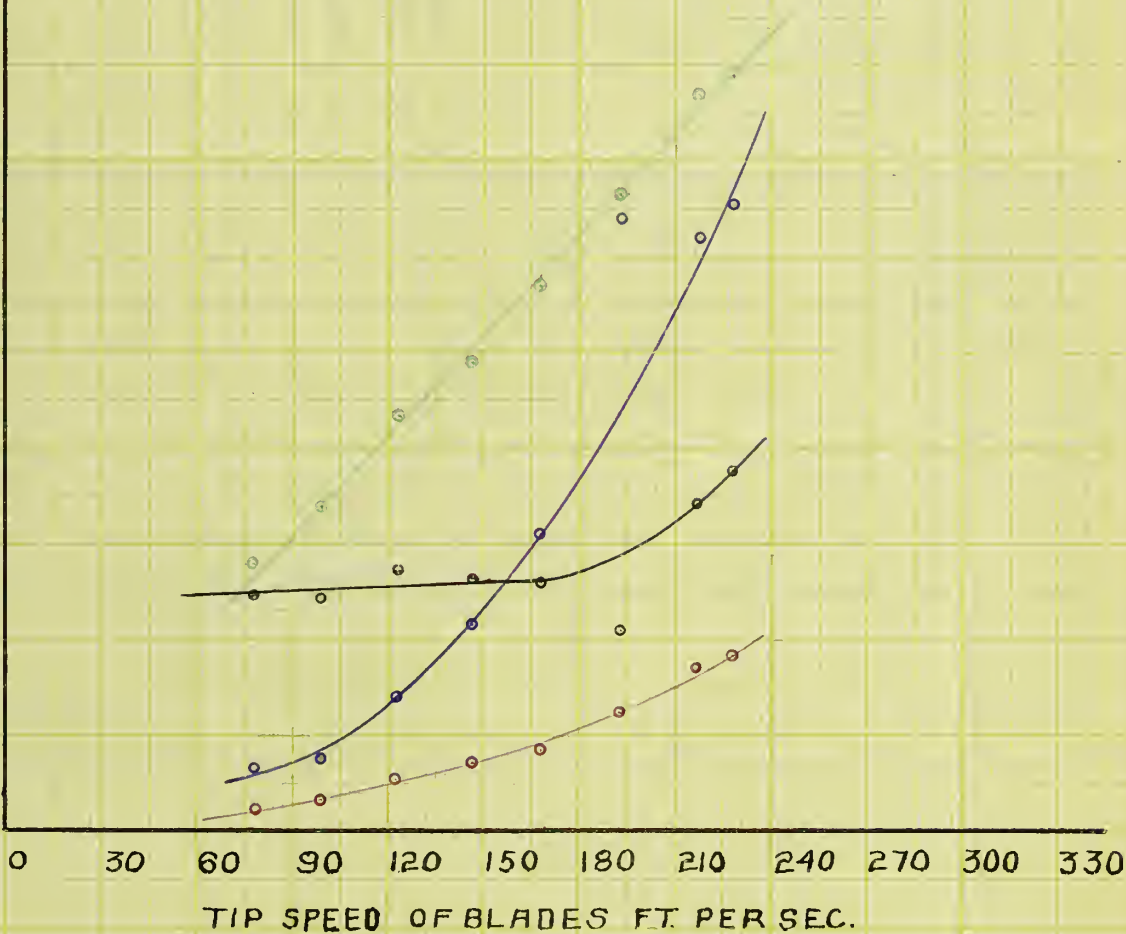


TABLE 3.

DATA AND RESULTS
FOR
BUFFALO BLOWER NO 8.
1/2 OPENING
OF
DISCHARGE

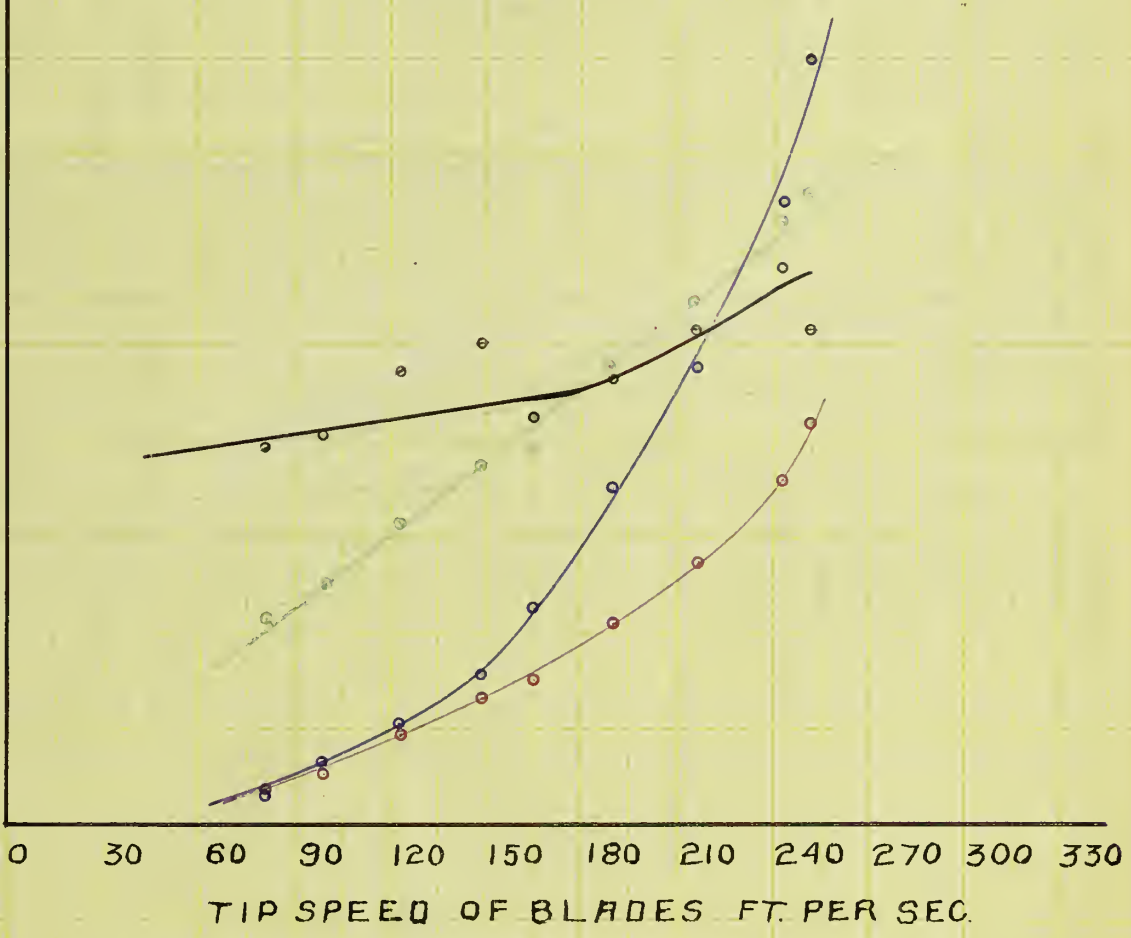
[illegible]

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 3.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

VOLUME
EFFICIENCY
H.P.
PRESSURE



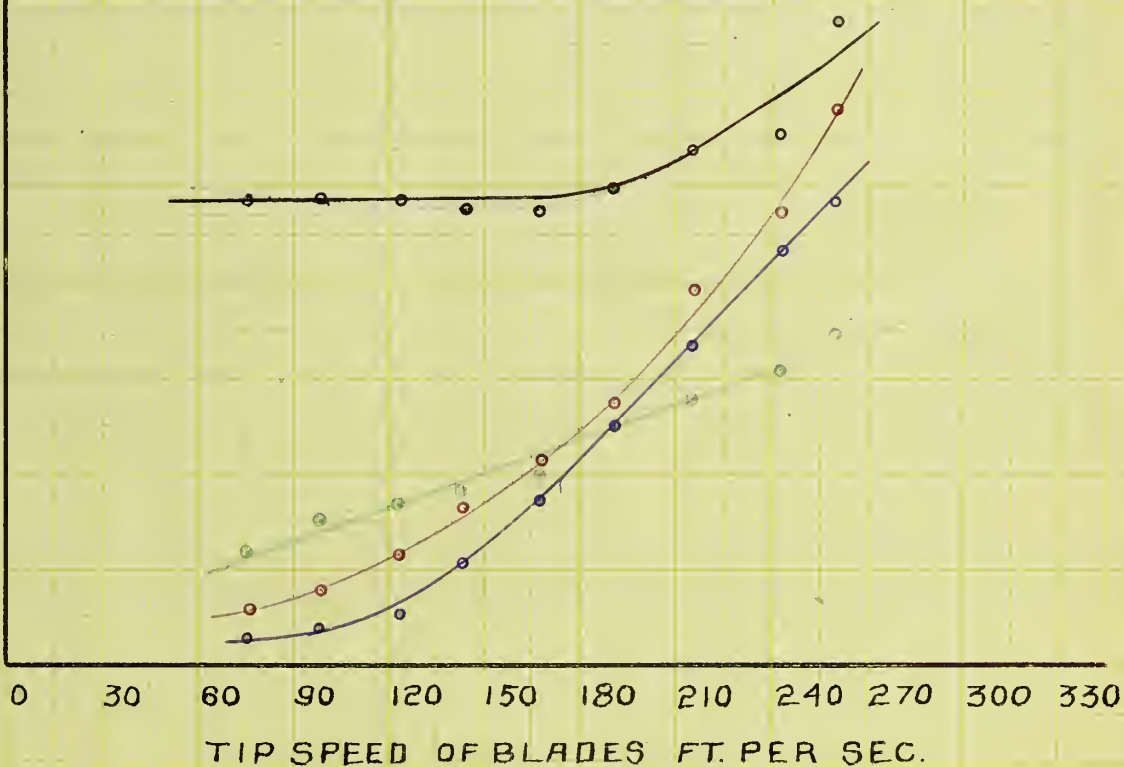
[illegible]

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 4.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE.

200
100
40
20
180
90
36
16
140
70
28
12
100
50
20
80
40
16
60
30
12
40
20
8
20
10
4
0
0
0
0

VOLUME
EFFICIENCY
H.P.
PRESSURE



[illegible]

1. The first part of the paper
 is devoted to the study of the
 properties of the function
 defined by the formula

(1)

where

is a function

1	0.0000
2	0.0000
3	0.0000
4	0.0000
5	0.0000
6	0.0000
7	0.0000
8	0.0000
9	0.0000
10	0.0000
11	0.0000
12	0.0000
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14	0.0000
15	0.0000
16	0.0000
17	0.0000
18	0.0000
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88	0.0000
89	0.0000
90	0.0000
91	0.0000
92	0.0000
93	0.0000
94	0.0000
95	0.0000
96	0.0000
97	0.0000
98	0.0000
99	0.0000
100	0.0000

The function is defined by the formula

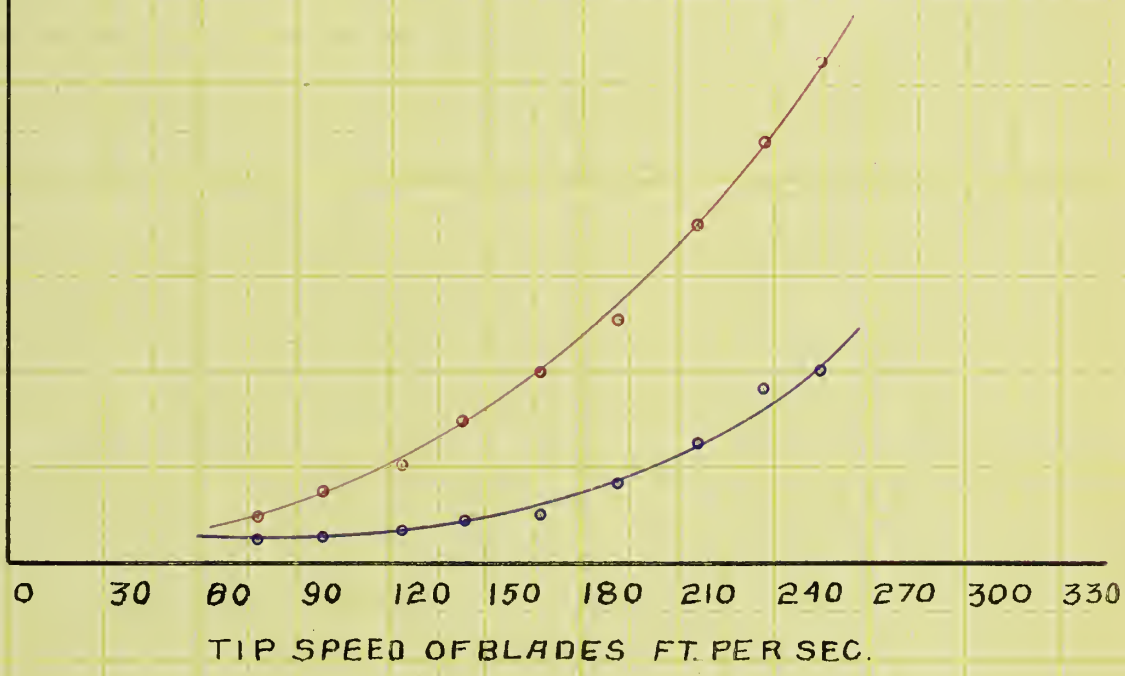
where

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 5.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

H.P.
PRESSURE



EXPERIMENT NO. 2

Buffalo Pressure Blower No. 7.

The general appearance of this blower is the same as that of No. 8 (See Plate III, page 40.) except that it has two driving pulleys and that its blast wheel is built with ten blades, five large and five small ones. The small blades are about one third the size of the large ones, between which they are placed, being riveted to the outer conical rim of the blast wheel.

Table of Dimensions:—

Height Total	33.5"
Length " "	34"
Width " "	30.75"
Diam. of Pulleys	5"

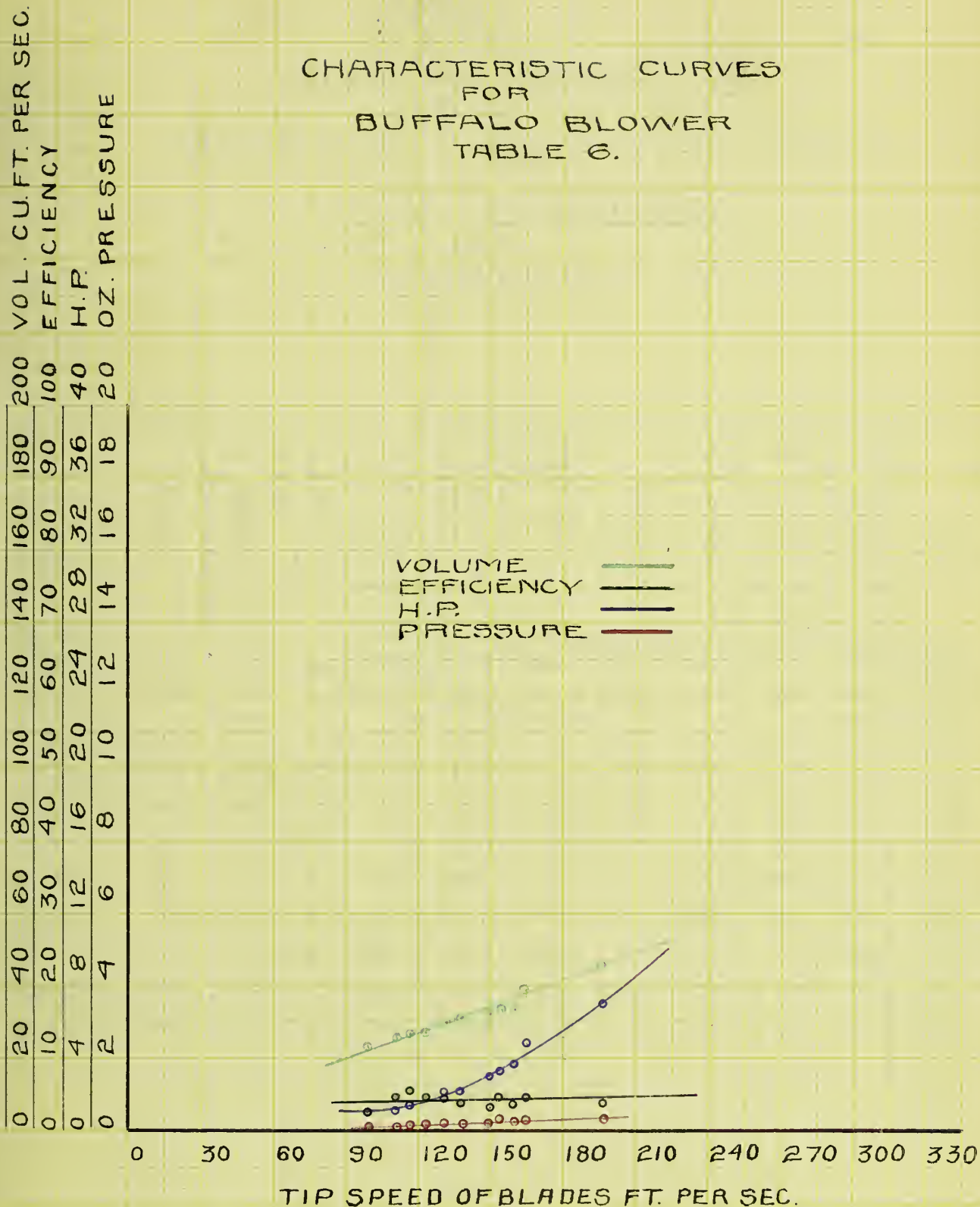
Face of Pulleys		$4\frac{5}{8}"$
diam. of Shaft		$1\frac{3}{8}"$
diam. of Blast Wheel		$17\frac{1}{4}"$
Width of " " at {	center	$5\frac{3}{8}"$
	Circ.	$2\frac{1}{4}"$
No. of Blades	{ Long	5
	{ Short	5
Area of Blades		11.7 sq.in.
diam. of Discharge Opening		$6\frac{7}{8}"$
Area " " " "		$37\frac{1}{8}$ sq.in.
diam. of Inlets		9"
Area " " "		127.24 sq.in.
Ratio $\frac{\text{Inlet Area}}{\text{Outlet Area}}$		2.3

The area of the pulleys were subtracted from the inlet area as they obstructed the openings.

Temperature and Barometer Readings.

Barometer (average)	$29.3"$
Temperature " "	$79\frac{1}{4}^{\circ}\text{F}$

CHARACTERISTIC CURVES
FOR
BUFFALO BLOWER
TABLE 6.

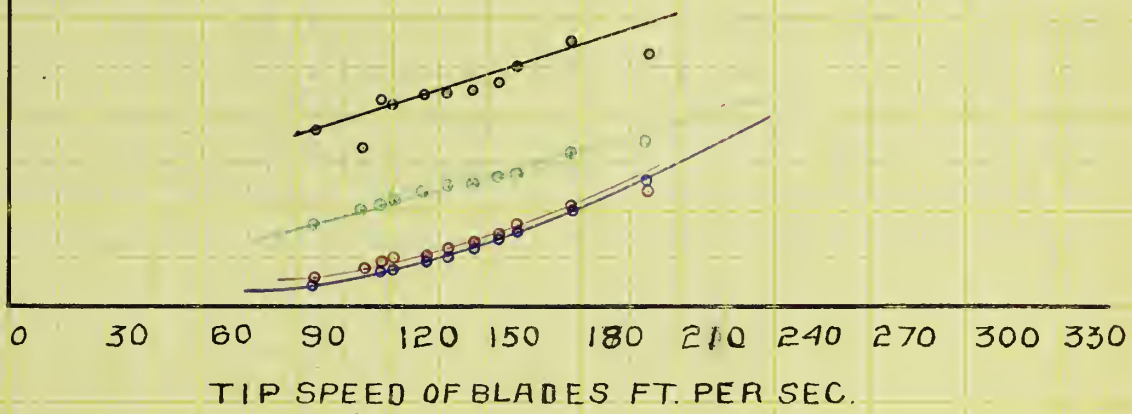


CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 7.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

200 180 160 140 120 100 80 60 40 20 0
100 90 80 70 60 50 40 30 20 10 0
40 36 32 28 24 20 16 12 8 4 0
20 18 16 14 12 10 8 6 4 2 0

VOLUME
EFFICIENCY
H.P.
PRESSURE

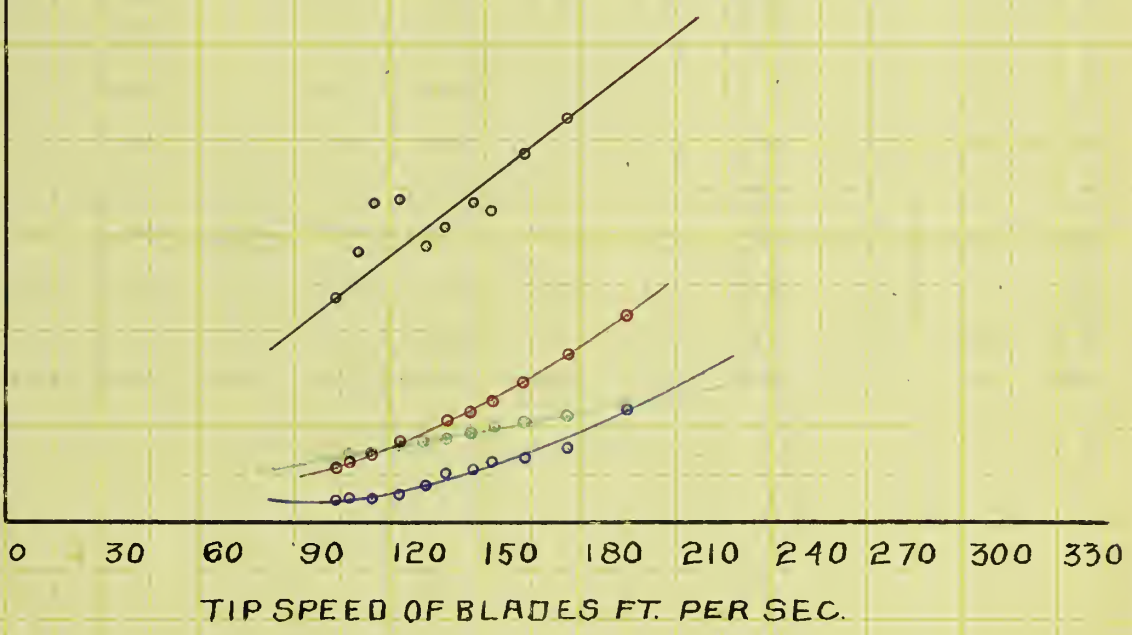


CHARACTERISTIC CURVES
FOR
BUFFALO BLOWER
TABLE 8.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

VOLUME
EFFICIENCY
H.P.
PRESSURE



CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 9.

VOL. CU. FT. PER SEC.										EFFICIENCY										H.P.										OZ. PRESSURE													
0	20	40	60	80	100	120	140	160	180	200	0	10	20	30	40	50	60	70	80	90	100	0	4	8	12	16	20	24	28	32	36	40	0	2	4	6	8	10	12	14	16	18	20

VOLUME
EFFICIENCY
H.P.
PRESSURE



1. The first part of the paper is devoted to a general discussion of the problem.

1. Introduction

No.	Date	Name	Age	Sex	Height	Weight	Blood Pressure	Heart Rate	Respiration Rate
1	1910	John	25	M	5' 10"	160	120/80	72	18
2	1910	John	25	M	5' 10"	160	120/80	72	18
3	1910	John	25	M	5' 10"	160	120/80	72	18
4	1910	John	25	M	5' 10"	160	120/80	72	18
5	1910	John	25	M	5' 10"	160	120/80	72	18
6	1910	John	25	M	5' 10"	160	120/80	72	18
7	1910	John	25	M	5' 10"	160	120/80	72	18
8	1910	John	25	M	5' 10"	160	120/80	72	18
9	1910	John	25	M	5' 10"	160	120/80	72	18
10	1910	John	25	M	5' 10"	160	120/80	72	18
11	1910	John	25	M	5' 10"	160	120/80	72	18
12	1910	John	25	M	5' 10"	160	120/80	72	18
13	1910	John	25	M	5' 10"	160	120/80	72	18
14	1910	John	25	M	5' 10"	160	120/80	72	18
15	1910	John	25	M	5' 10"	160	120/80	72	18
16	1910	John	25	M	5' 10"	160	120/80	72	18
17	1910	John	25	M	5' 10"	160	120/80	72	18
18	1910	John	25	M	5' 10"	160	120/80	72	18
19	1910	John	25	M	5' 10"	160	120/80	72	18
20	1910	John	25	M	5' 10"	160	120/80	72	18

TABLE 10.

DATA AND RESULTS
FOR
BUFFALO BLOWER NO 7.

O OPENING
OF
DISCHARGE

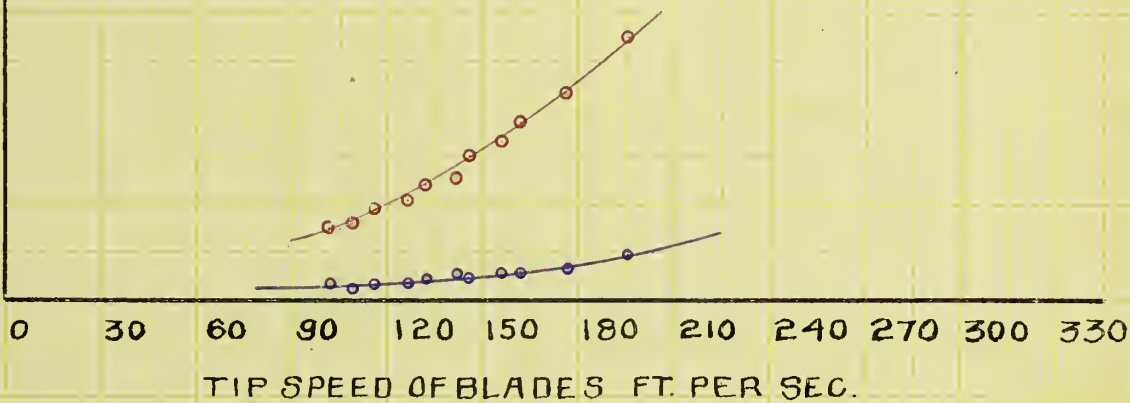
[illegible]

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 10

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE.

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

H.P.
PRESSURE



TIP SPEED OF BLADES FT. PER SEC.

THE HISTORY OF THE

REIGN OF

EXPERIMENT NO. 3

Buffalo Volume Blower No 4.

The appearance and details of this blower are identically the same as those of Volume Blower No 8 (See Plate III page 40, and description of No. 8 page 37.) The only difference in the two blowers is that of size.

Table of Dimensions:—

Height Total	28"
Length " "	27½"
Width " "	29⅜"
Diam. of Pulley	5"
Face " " "	4"
Diam. of Shaft	1¼"
Diam. of Blast Wheel	16¼"
Width " " " at { Circ,	4¼"
	{ Center 6⅞"

No of Blades	5
Size " "	
Area " " "	19.3 sq. in.
Diam. of Discharge Opening	8 1/2"
Area " " " " "	56 3/4 sq. in.
Diam. " Inlets (two)	8"
Area " " "	100.5 sq. in.
Ratio $\frac{\text{Inlet Area}}{\text{Outlet Area}} =$	1.2

Temperature and Barometer Readings

Barometer (corragr)	29.76"
Temperature " "	76.54° F.

TABLE II.

DATA AND RESULTS
FOR
BUFFALO BLOWER NO 4.

FULL OPENING
OF
DISCHARGE

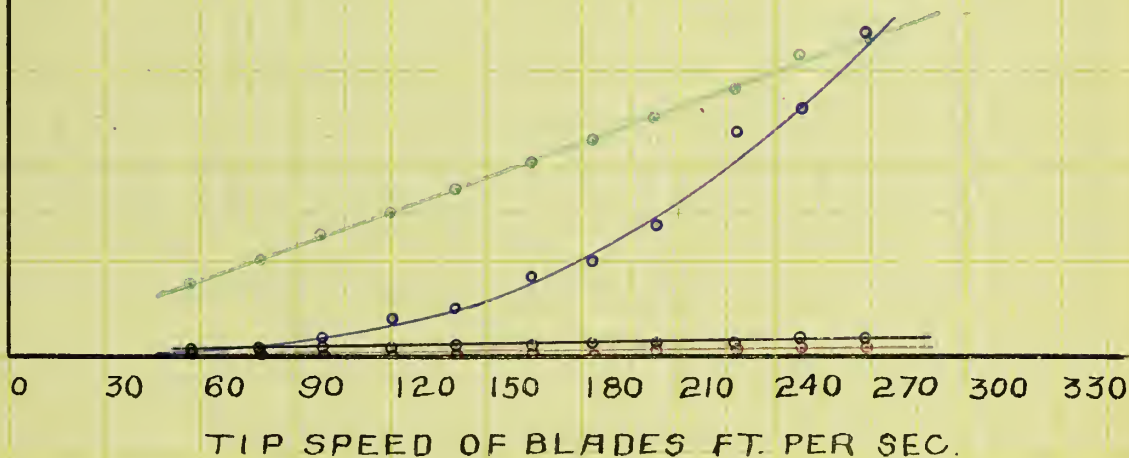
[illegible]

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE II.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE.

200
180
160
140
120
100
80
60
40
20
0
200
180
160
140
120
100
80
60
40
20
0
200
180
160
140
120
100
80
60
40
20
0

VOLUME
EFFICIENCY
H.P.
PRESSURE



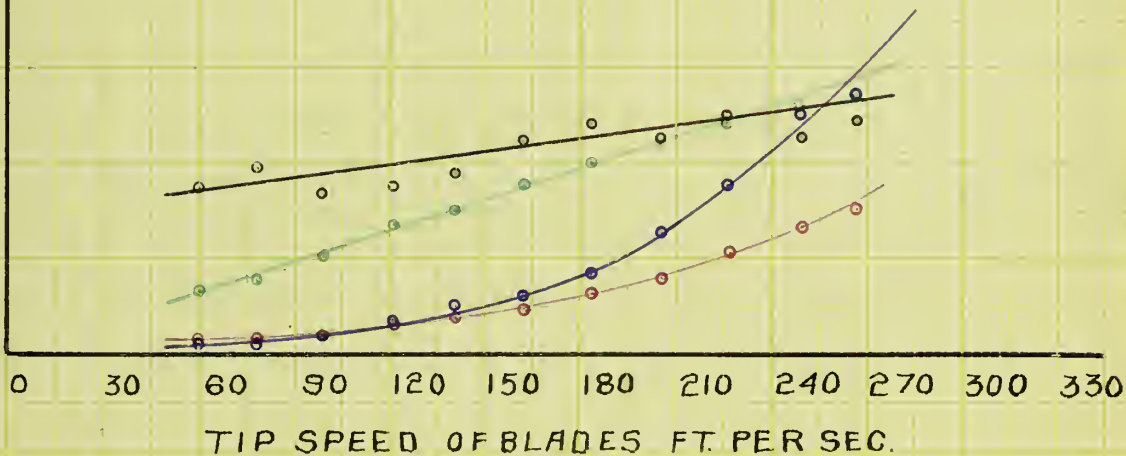
TIP SPEED OF BLADES FT. PER SEC.

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 12.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

200
100
40
20
180
90
36
18
160
80
32
16
140
70
28
14
120
60
24
12
100
50
20
10
80
40
16
8
60
30
12
6
40
20
8
4
20
10
4
2
0
0
0
0

VOLUME
EFFICIENCY
H.P.
PRESSURE



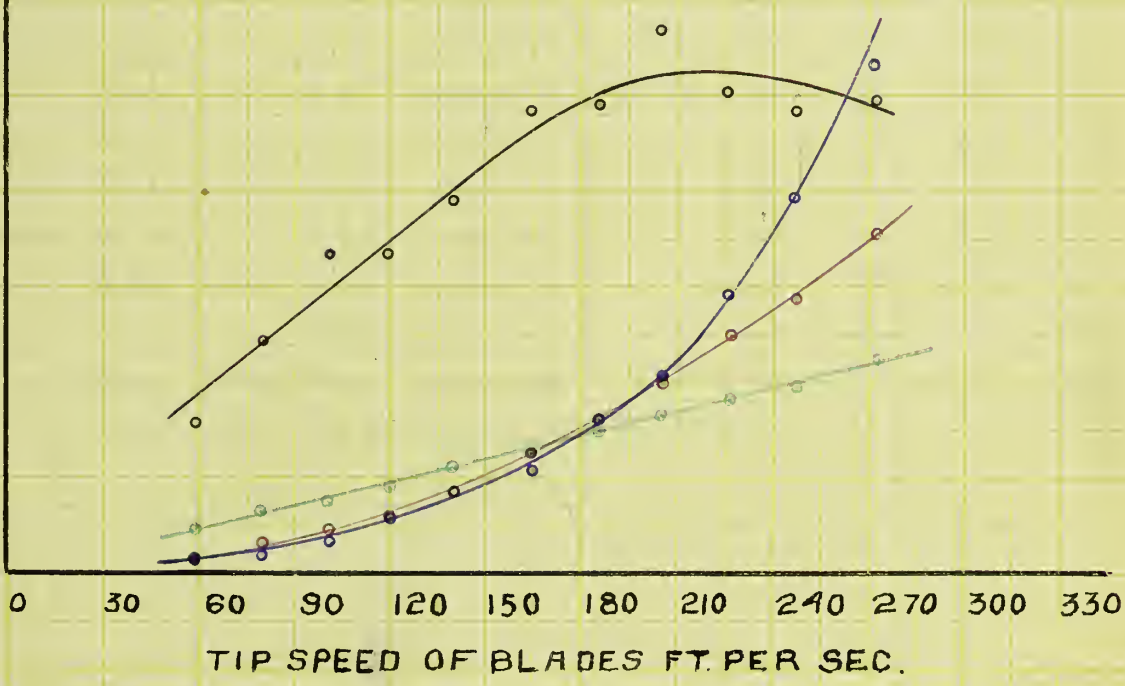
TIP SPEED OF BLADES FT. PER SEC.

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 13.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

VOLUME
EFFICIENCY
H.P.
PRESSURE



TIP SPEED OF BLADES FT. PER SEC.

TABLE 14.

DATA AND RESULTS
FOR
BUFFALO BLOWER NO 4.

$\frac{1}{4}$ OPENING
OF
DISCHARGE

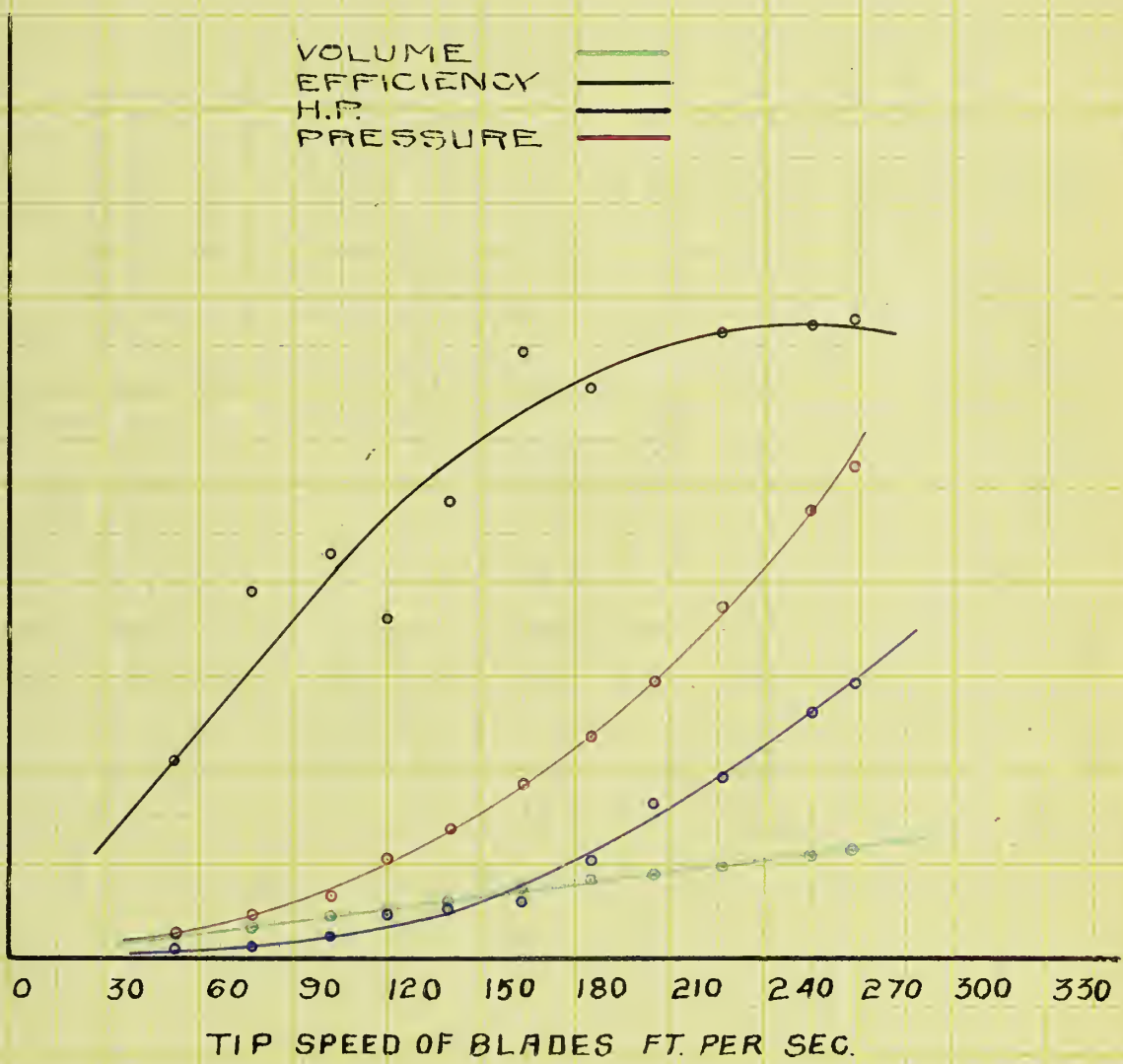
[illegible]

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 14

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

200	180	160	140	120	100	80	60	40	20	0
100	90	80	70	60	50	40	30	20	10	0
40	36	32	28	24	20	16	12	8	4	0
20	18	16	14	12	10	8	6	4	2	0

VOLUME
EFFICIENCY
H.P.
PRESSURE



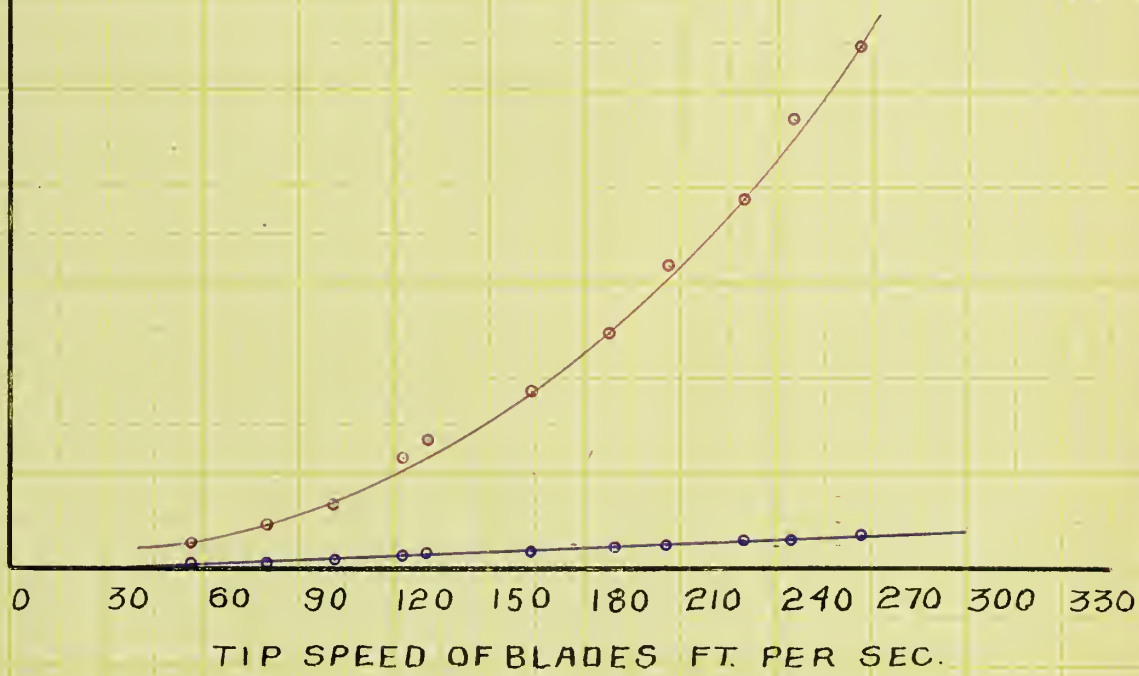
TIP SPEED OF BLADES FT. PER SEC.

CHARACTERISTIC CURVES FOR BUFFALO BLOWER TABLE 15.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

VOLUME
EFFICIENCY
H.P.
PRESSURE



EXPERIMENT NO.4

Sturtevant Blower No 1.

See Plate 4 page 81:— This is the smallest size of Pressure Blower built for the general trade and is suitable for all purposes where a small volume of air at a pressure of from five to ten ounces is desired. Its casing, constructed of cast iron has two inlet openings. The blast wheel is constructed ^{almost} entirely of steel sheet-iron, there being twelve blades riveted to conical side plates and the whole carried by and fastened to the hub by means of steel spokes, in the same way that a bicycle rim is fastened to its hub. The blades are curved from the hub

to the rim of the wheel, in the form of a spiral.

Table of Dimensions:

Height Total	22 $\frac{1}{2}$ "
Length " "	23 $\frac{1}{2}$ "
Width " "	14"
Diam. of Pulleys	3"
Face " " "	2 $\frac{3}{8}$ "
Diam. " Shaft	7 $\frac{1}{16}$ "
Width of Blast Wheel	<div> <div> Outer Circ. </div> <div> $\frac{1}{2}$" $3 \frac{1}{2}$" </div> </div>
Diam. " " " " "	12"
No. of Blades	12
Size " " "	4" x 1 $\frac{1}{2}$ " x 2 $\frac{1}{2}$ "
Area " " "	8 sq. in.
Diam. of Discharge Opening	4 $\frac{1}{4}$ "
Area " " " " "	14.18 sq. in.
Diam. of Inlets	5"

Area of Inlets (two)

37.77 sq. in.

Ratio $\frac{\text{Inlet Area}}{\text{Outlet Area}} =$

1.7

Temperature and Barometer Readings.

Barometer Height Av.

29.9

Temperature Av.

80°F.

PLATE IV.
STURTEVANT BLOWER
NUMBER 1.
WITH
BLAST WHEEL

BLAST WHEEL
SCALE $\frac{3}{16}'' = 1''$

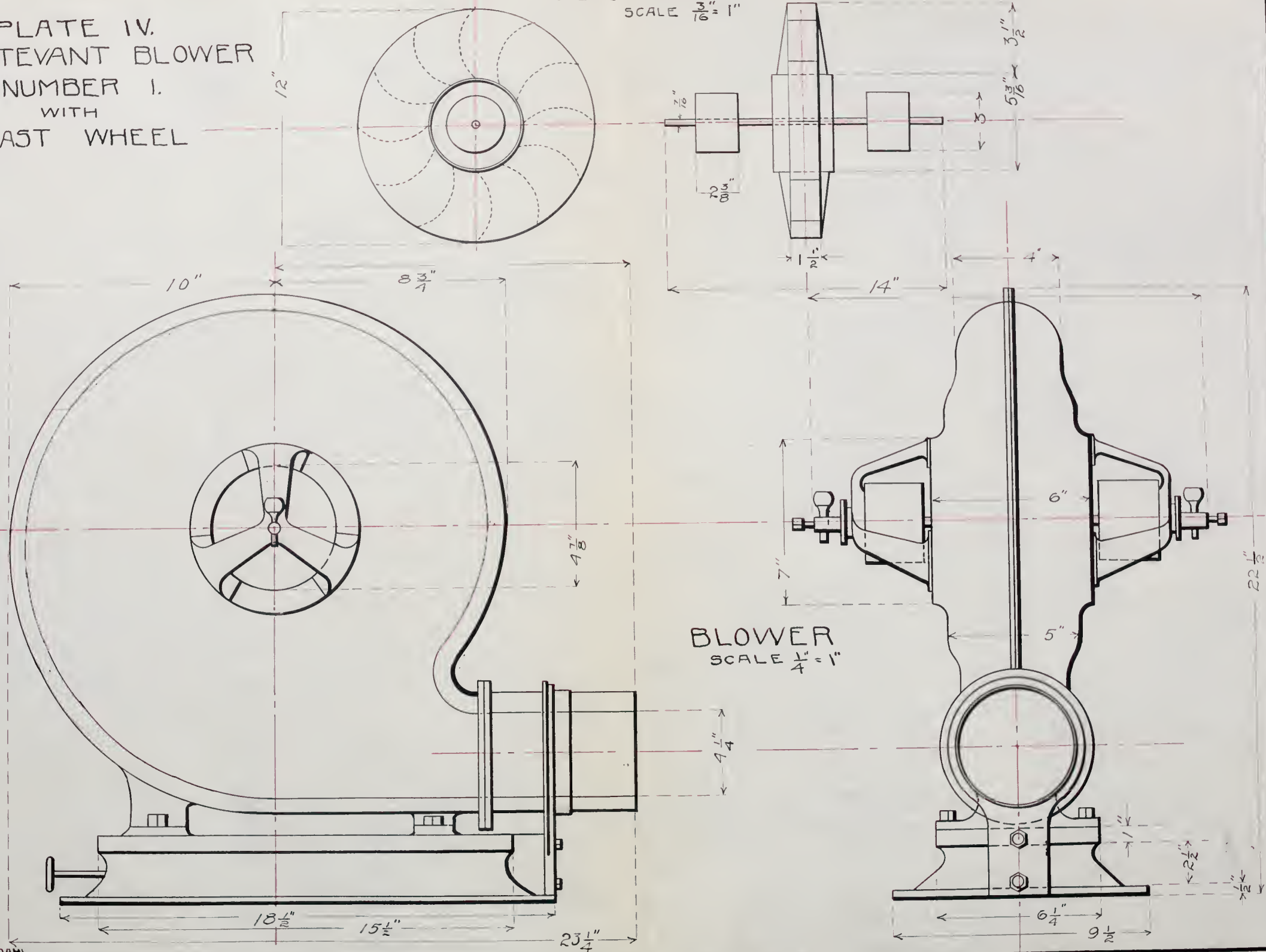


TABLE 16.

DATA AND RESULTS
FOR
STURTEVANT BLOWYER NO 1.
FULL OPENING
OF
DISCHARGE

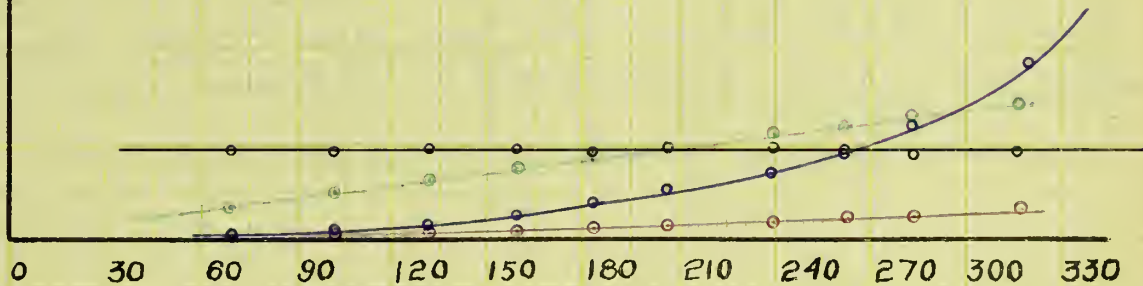
R.P.M. FAN	R.P.M. ENG	PRESSURE OZ. PER SQ. IN	VEL. HEAD IN WATER	VEL. OF AIR FT. PER SEC.	AIR DISCH CU. FT. PER SEC.	VEL. FAN TIPS FT. PER SEC.	H.P. TOTAL	H.P. TO DRIVE FAN	H.P. THEORETICAL	CU. FT. AIR DISCH. PER H.P. PER SEC.	EFF. O/O.
1350	52	.08	.32	38.2	6.7	70.8	.38	.18	.01	32.0	4.5
2048	80	.13	.73	57.7	10.2	102	.82	.48	.02	21.0	4.5
2524	98	.14	1.17	72.7	12.8	132	1.17	.64	.03	20.5	4.6
3060	120	.19	1.54	83.8	14.8	160	1.76	1.01	.05	14.7	4.6
3504	137	.25	2.09	97.7	17.2	184	2.20	1.65	.07	10.4	4.2
3960	150	.32	2.60	109.2	19.2	207	3.25	2.07	.11	9.3	4.8
4508	176	.36	3.41	124.5	21.9	240	4.26	2.76	.13	7.9	4.7
5034	200	.42	3.97	134.5	23.6	263	5.85	3.85	.16	6.1	4.2
5440	214	.44	4.78	148.0	26.1	284	6.99	4.74	.19	5.5	4.0
6080	238	.56	5.61	160.0	28.2	318	8.90	6.11	.26	4.6	4.2
6470	266	.66	6.08	167.0	29.4	388	11.17	7.57	.32	3.8	4.2

CHARACTERISTIC CURVES FOR STURTEVANT BLOWER TABLE 16.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

VOLUME
EFFICIENCY
H.P.
PRESSURE



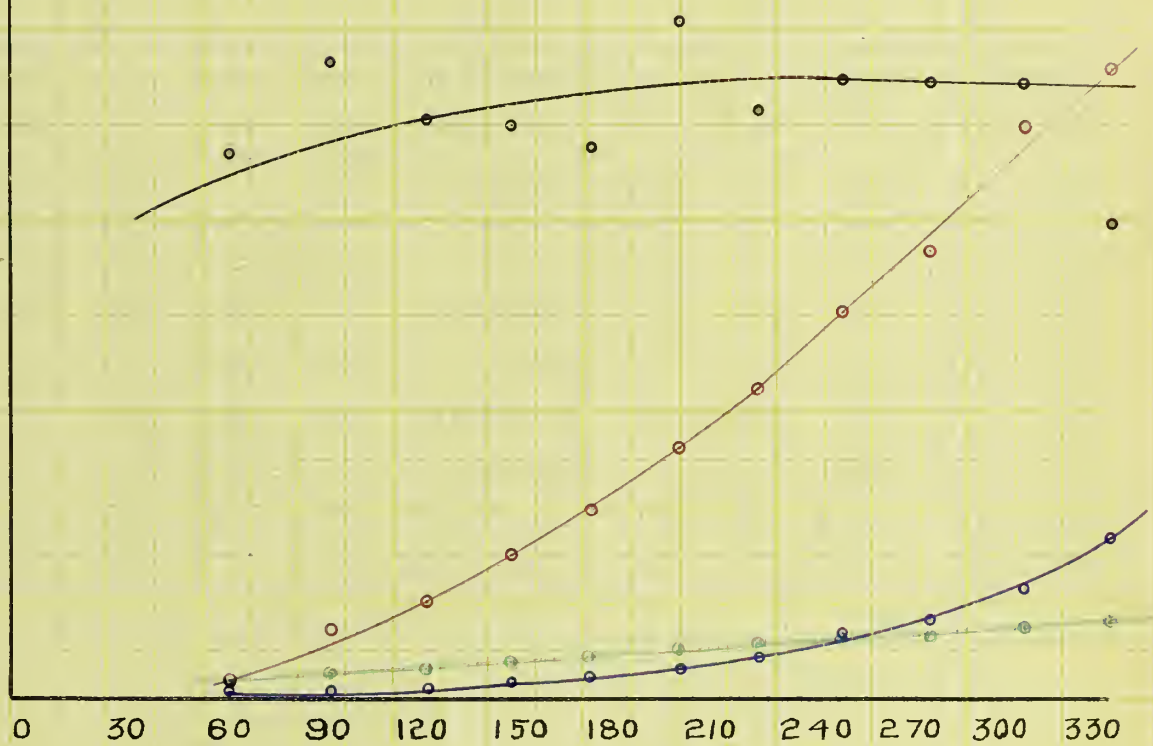
TIP SPEED OF BLADES FT. PER SEC.

CHARACTERISTIC CURVES FOR STURTEVANT BLOWER TABLE 17.

VOL CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

VOLUME
EFFICIENCY
H.P.
PRESSURE



TIP SPEED OF BLADES FT. PER SEC.

[illegible]

1800 1810 1820 1830 1840 1850 1860 1870 1880 1890 1900 1910 1920 1930 1940 1950 1960 1970 1980 1990 2000

2

1800 1810 1820 1830 1840 1850 1860 1870 1880 1890 1900 1910 1920 1930 1940 1950 1960 1970 1980 1990 2000

1800	1810	1820	1830	1840	1850	1860	1870	1880	1890	1900	1910	1920	1930	1940	1950	1960	1970	1980	1990	2000
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42
43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63
64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84
85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105
106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126
127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147
148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168
169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189
190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210
211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231
232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252
253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273
274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294
295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315
316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336
337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357
358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378
379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399
400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420
421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441
442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462
463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	480	481	482	483
484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	500	501	502	503	504
505	506	507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	523	524	525
526	527	528	529	530	531	532	533	534	535	536	537	538	539	540	541	542	543	544	545	546
547	548	549	550	551	552	553	554	555	556	557	558	559	560	561	562	563	564	565	566	567
568	569	570	571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588
589	590	591	592	593	594	595	596	597	598	599	600	601	602	603	604	605	606	607	608	609
610	611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630
631	632	633	634	635	636	637	638	639	640	641	642	643	644	645	646	647	648	649	650	651
652	653	654	655	656	657	658	659	660	661	662	663	664	665	666	667	668	669	670	671	672
673	674	675	676	677	678	679	680	681	682	683	684	685	686	687	688	689	690	691	692	693
694	695	696	697	698	699	700	701	702	703	704	705	706	707	708	709	710	711	712	713	714
715	716	717	718	719	720	721	722	723	724	725	726	727	728	729	730	731	732	733	734	735
736	737	738	739	740	741	742	743	744	745	746	747	748	749	750	751	752	753	754	755	756
757	758	759	760	761	762	763	764	765	766	767	768	769	770	771	772	773	774	775	776	777
778	779	780	781	782	783	784	785	786	787	788	789	790	791	792	793	794	795	796	797	798
799	800	801	802	803	804	805	806	807	808	809	810	811	812	813	814	815	816	817	818	819
820	821	822	823	824	825	826	827	828	829	830	831	832	833	834	835	836	837	838	839	840
841	842	843	844	845	846	847	848	849	850	851	852	853	854	855	856	857	858	859	860	861
862	863	864	865	866	867	868	869	870	871	872	873	874	875	876	877	878	879	880	881	882
883	884	885	886	887	888	889	890	891	892	893	894	895	896	897	898	899	900	901	902	903
904	905	906	907	908	909	910	911	912	913	914	915	916	917	918	919	920	921	922	923	924
925	926	927	928	929	930	931	932	933	934	935	936	937	938	939	940	941	942	943	944	945
946	947	948	949	950	951	952	953	954	955	956	957	958	959	960	961	962	963	964	965	966
967	968	969	970	971	972	973	974	975	976	977	978	979	980	981	982	983	984	985	986	987
988	989	990	991	992	993	994	995	996	997	998	999	1000	1001	1002	1003	1004	1005	1006	1007	1008
1009	1010	1011	1012	1013	1014	1015	1016	1017	1018	1019	1020	1021	1022	1023	1024	1025	1026	1027	1028	1029
1030	1031	1032	1033	1034	1035	1036	1037	1038	1039	1040	1041	1042	1043	1044	1045	1046	1047	1048	1049	1050
1051	1052	1053	1054	1055	1056	1057	1058	1059	1060	1061	1062	1063	1064	1065	1066	1067	1068	1069	1070	1071
1072	1073	1074	1075	1076	1077	1078	1079	1080	1081	1082	1083	1084	1085	1086	1087	1088	1089	1090	1091	1092
1093	1094	1095	1096	1097	1098	1099	1100	1101	1102	1103	1104	1105	1106	1107	1108	1109	1110	1111	1112	1113
1114	1115	1116	1117	1118	1119	1120	1121	1122	1123	1124	1125	1126	1127	1128	1129	1130	1131	1132	1133	1134
1135	1136	1137	1138	1139	1140	1141	1142	1143	1144	1145	1146	1147	1148	1149	1150	1151	1152	1153	1154	1155
1156	1157	1158	1159	1160	1161	1162	1163	1164	1165	1166	1167	1168	1169	1170	1171	1172	1173	1174	1175	1176
1177	1178	1179	1180	1181	1182	1183	1184	1185	1186	1187	1188	1189	1190	1191	1192	1193	1194	1195	1196	1197
1198	1199	1200	1201	1202	1203	1204	1205	1206	1207	1208	1209	1210	1211	1212	1213	1214	1215	1216	1217	1218
1219	1220	1221	1222	1223	1224	1225	1226	1227	1228	1229	1230	1231	1232	1233	1234	1235	1236	1237	1238	1239
1240	1241	1242	1243	1244	1245	1246	1247	1248	1249	1250	1251	1252	1253	1254	1255	1256	1257	1258	1259	1260
1261	1262	1263	1264	1265	1266	1267	1268	1269	1270	1271	1272	1273	1274	1275	1276	1277	1278	1279	1280	1281
1282	1283	1284	1285	1286	1287	1288	1289	1290	1291	1292	1293	1294	1295	1296	1297	1298	1299	1300	1301	1302
1303	1304	1305	1306	1307	1308	1309	1310	1311	1312	1313	1314	1315	1316	1317	1318	1319	1320	1321	1322	1323
1324	1325	1326	1327	1328	1329	1330	1331	1332	1333	1334	1335	1336	1337	1338	1339	1340	1341	1342	1343	1344
1345	1346	1347	1348	1349	1350	1351	1352	1353	1354	1355	1356	1357	1358	1359	1360	1361	1362	1363	1364	1365
1366	1367	1368	1369	1370	1371	1372	1373	1374	1375	1376	1377	1378	1379	1380	1381	1382	1383	1384	1385	1386
1387	1388	1389	1390	1391	1392	1393	1394	1395	1396	1397	1398	1399	1400	1401	1402	1403	1404	1405	1406	1407
1408	1409	1410																		

CHARACTERISTIC CURVES FOR STURTEVANT BLOWER TABLE 18.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

200	180	160	140	120	100	80	60	40	20	0
100	90	80	70	60	50	40	30	20	10	0
40	36	32	28	24	20	16	12	8	4	0
20	18	16	14	12	10	8	6	4	2	0

VOLUME
EFFICIENCY
H.P.
PRESSURE



TABLE 19.
DATA AND RESULTS
STURTEVANT BLOWER NO 1.
O OPENING
OF
DISCHARGE

R.P.M. FAN	R.P.M. ENG	PRESSURE OZ. PER SQ. IN.	VEL HEAD IN. WATER	VEL OF AIR FT. PER. SEC.	AIR DISCH. CU. FT. PER SEC.	VEL. FAN TIPS FT. PER SEC.	H.P. TOTAL	H P TO DRIVE FAN	H.P. THEORETICAL	CU. FT. AIR DISCH. PER. H.P. PER. SEC.	EFF. O/O
1290	50	.74	0	0	0	68	.28	.03	0	0	0
2162	84	1.69	0	0	0	116	.58	.15	0	0	0
2580	100	2.37	0	0	0	134	.73	.18	0	0	0
3020	118	3.50	0	0	0	158	1.11	.39	0	0	0
3440	134	4.56	0	0	0	181	1.43	.53	0	0	0
4010	156	6.18	0	0	0	210	1.56	.36	0	0	0
4502	175	7.90	0	0	0	236	2.20	.69	0	0	0
5030	196	9.80	0	0	0	263	2.88	.98	0	0	0
5450	212	11.00	0	0	0	285	3.38	1.13	0	0	0
6120	238	14.50	0	0	0	320	5.07	2.22	0	0	0
6650	260	17.50	0	0	0	348	6.20	2.80	0	0	0
7050		19.20				369					

CHARACTERISTIC CURVES FOR STURTEVANT BLOWER TABLE 19.

VOL. CU. FT. PER SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

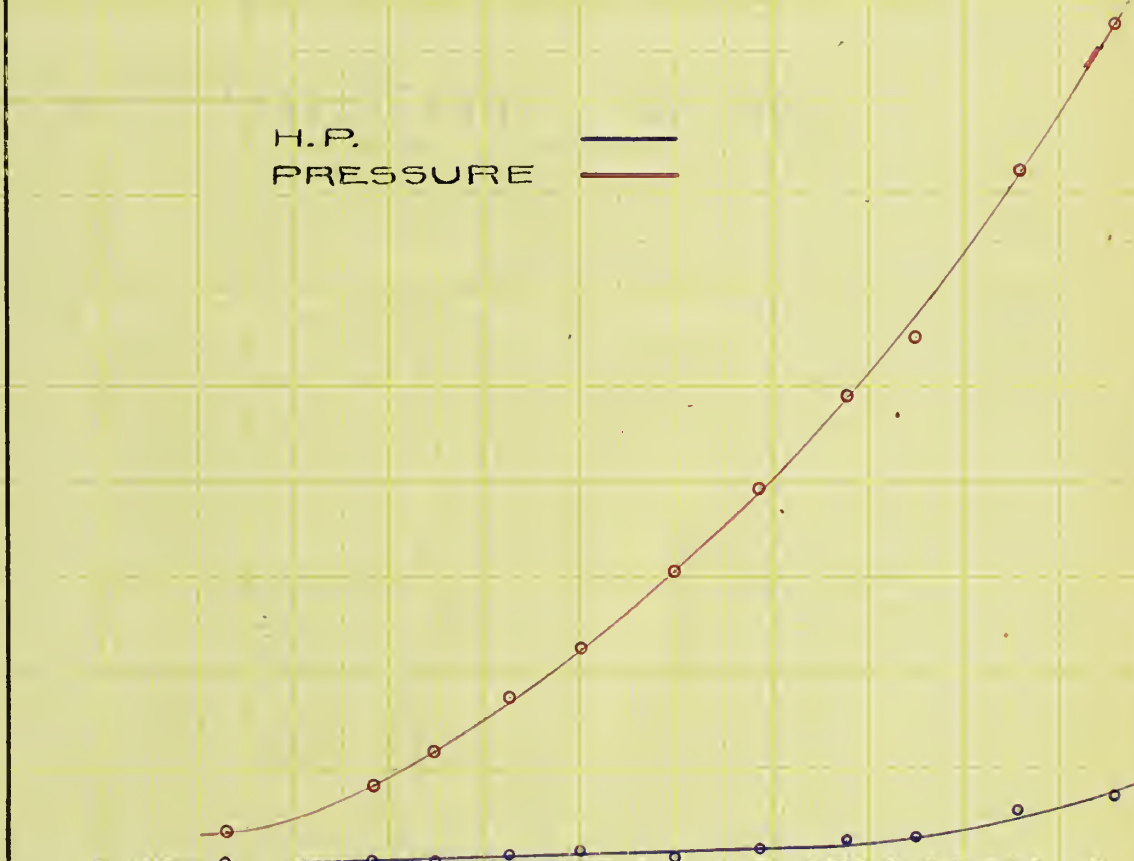
200	180	160	140	120	100	80	60	40	20	0
100	90	80	70	60	50	40	30	20	10	0
40	36	32	28	24	20	16	12	8	4	0
20	18	16	14	12	10	8	6	4	2	0

H.P.
PRESSURE

—
—

0 30 60 90 120 150 180 210 240 270 300 330

TIP SPEED OF BLADES FT. PER SEC.



EXPERIMENT NO. 5

35" Buffalo Exhauster.

See Plate 1, p. 94. This Buffalo Steel Plate Blowing Mill Exhauster was constructed of heavy steel plate firmly braced and stiffened with angle irons. A heavy cast iron pedestal, entirely independent of the fan shell, carried the pulley wheel and ring oiling bearings. The exhauster (like all exhausters) had a single inlet orifice and an overhung blast wheel. The latter consisted essentially of a cast iron hub with wrought iron spider arms, conical side plates and steel blades, the tips of which were slightly curved backward.

Table of Dimensions.

Height Total		$39\frac{3}{4}"$
Length " "		$36\frac{1}{4}"$
Width " "		$41\frac{3}{8}"$
Diam. of Pulley		8"
Face " " "		7"
Diam. of Shaft		$1\frac{3}{4}"$
Length of Bearings		$6\frac{3}{8}$ and $7\frac{3}{8}"$
Diam. of Blast Wheel at	{ Center	$12\frac{3}{4}"$
	{ Circ.	$9\frac{1}{2}"$
No. of Blades.		5
Area " " "		86.6 sq. in.
Size of Discharge Opening	{ Outside of Flange	$13\frac{3}{8}" \times 13\frac{1}{2}"$
	{ Inside " " "	$12" \times 13"$
Area " " " "	{ Outside of Flange	180 sq. in.
	{ Inside of Flange	169 sq. in.
Diam. of Inlet	{ Outside of Flange	$14\frac{5}{8}"$
	{ Inside " " "	$14\frac{1}{4}"$

Area of Inlet { Outside of Flange 167.9 sq. in.
 Inside " " " 159.5 sq. in.

$$\text{Ratio } \frac{\text{Inlet Area}}{\text{Outlet Area}} = .94$$

Temperature and Barometer Readings.

Barometer Height Av. 29.99 "

Temperature Av. 97 $\frac{5}{8}$ ° F.



PLATE V.
40" BUFFALO EXHAUSTER

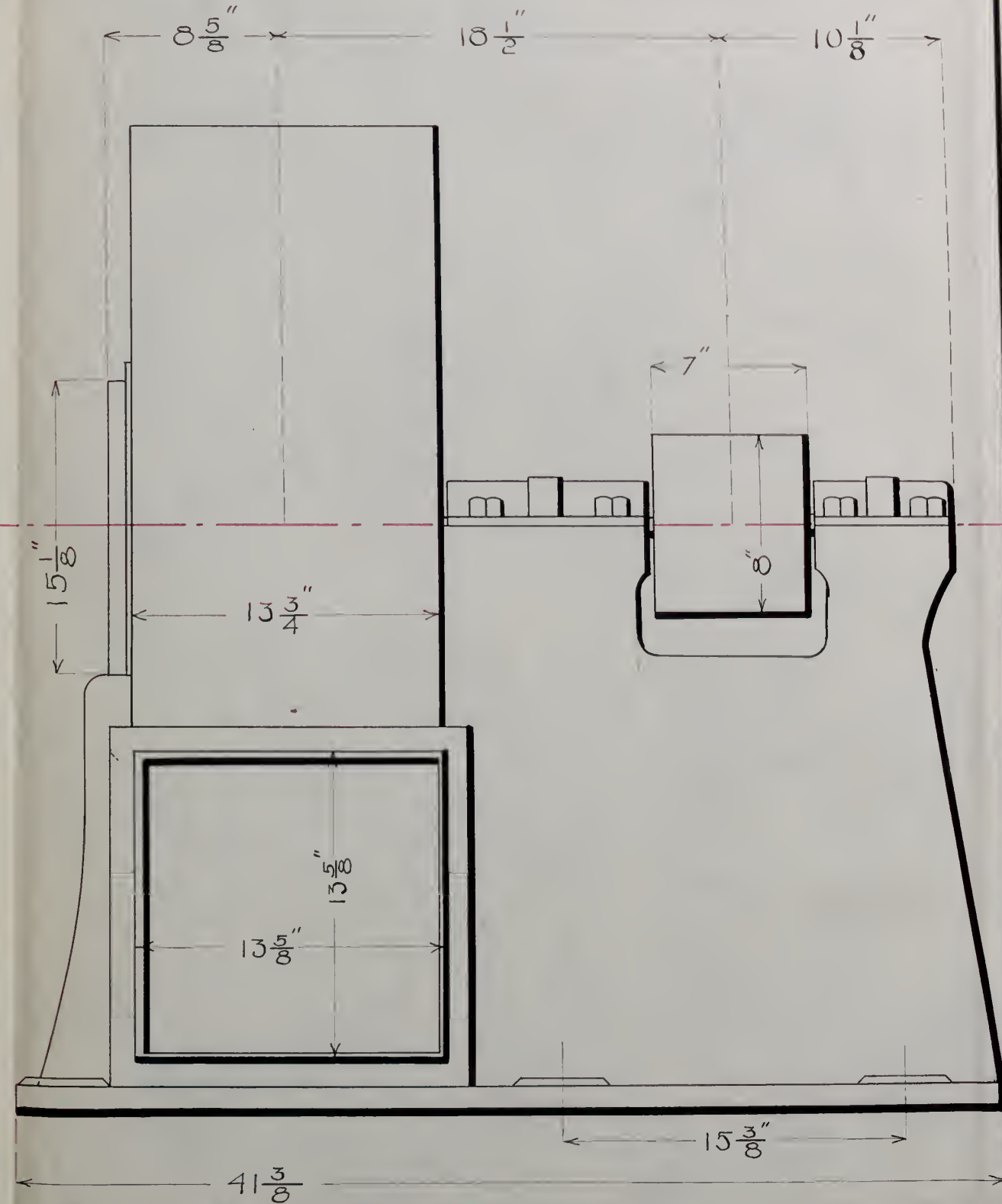
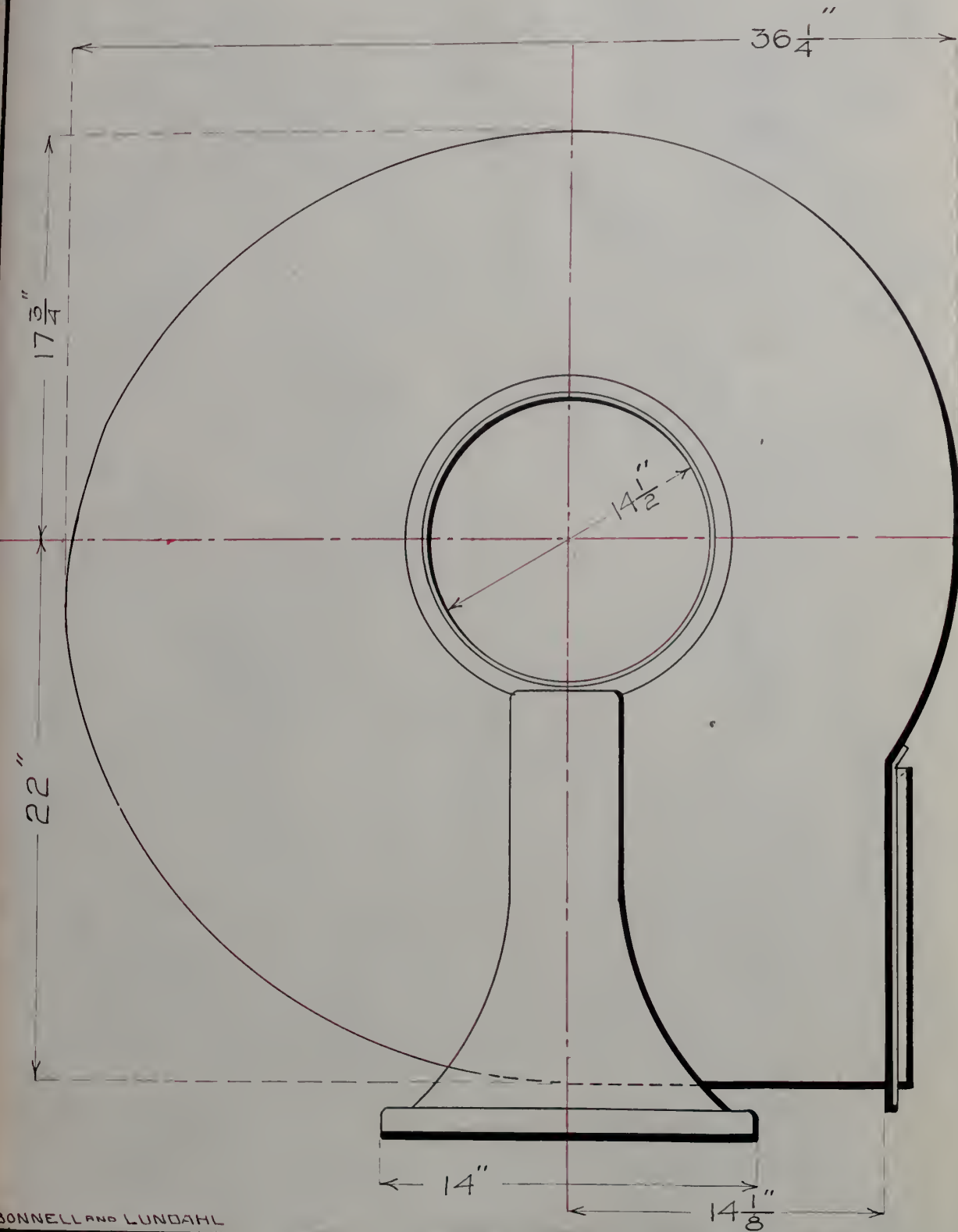
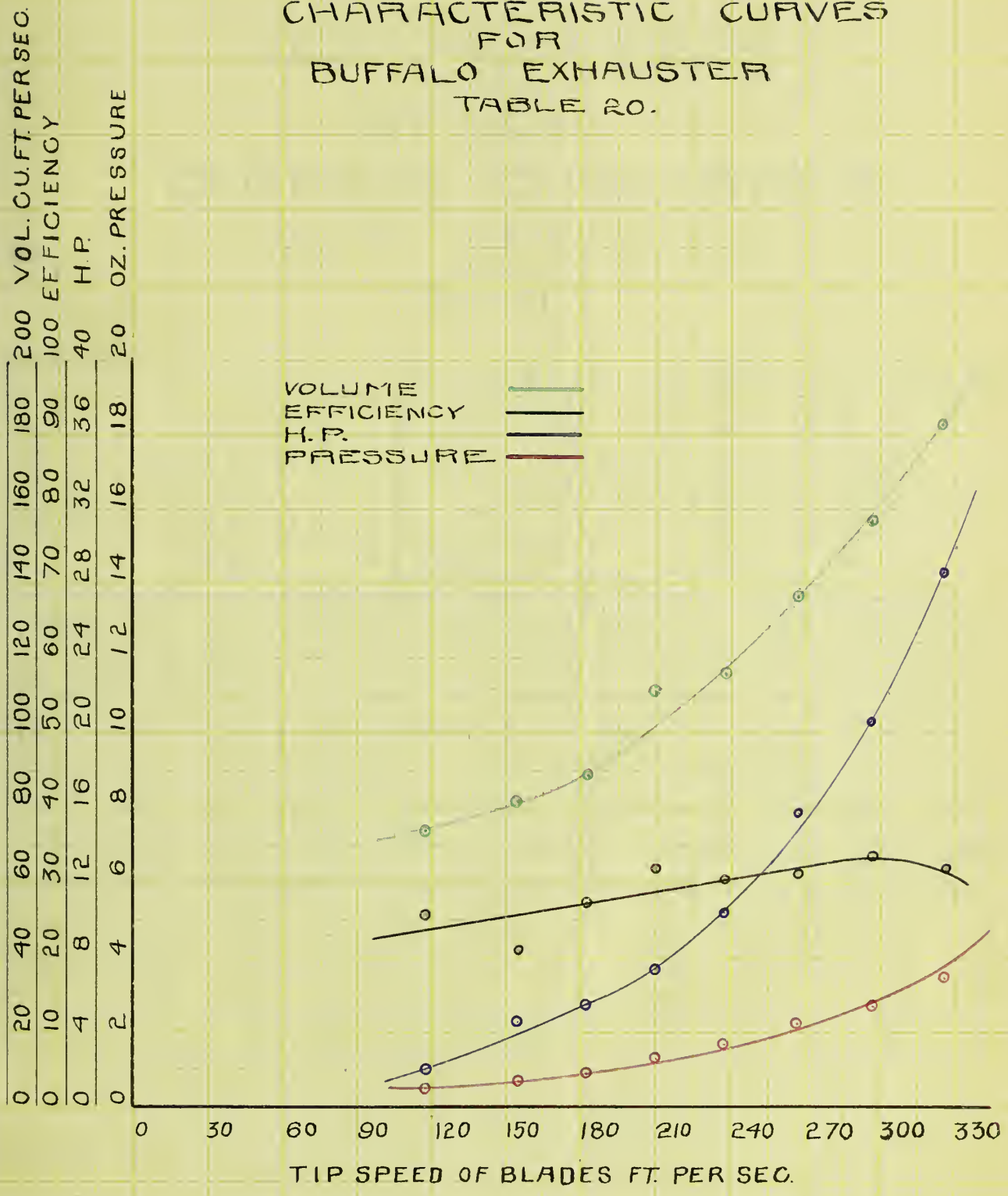


TABLE 20.

DATA AND RESULTS
FOR
40" INCH
BUFFALO EXHAUSTER
FULL OPENING
OF
INTAKE

[illegible]

CHARACTERISTIC CURVES
FOR
BUFFALO EXHAUSTER
TABLE 20.



1890

1891

1892

1893

1894

1895

1896

1897

1898

1899

1900

1901

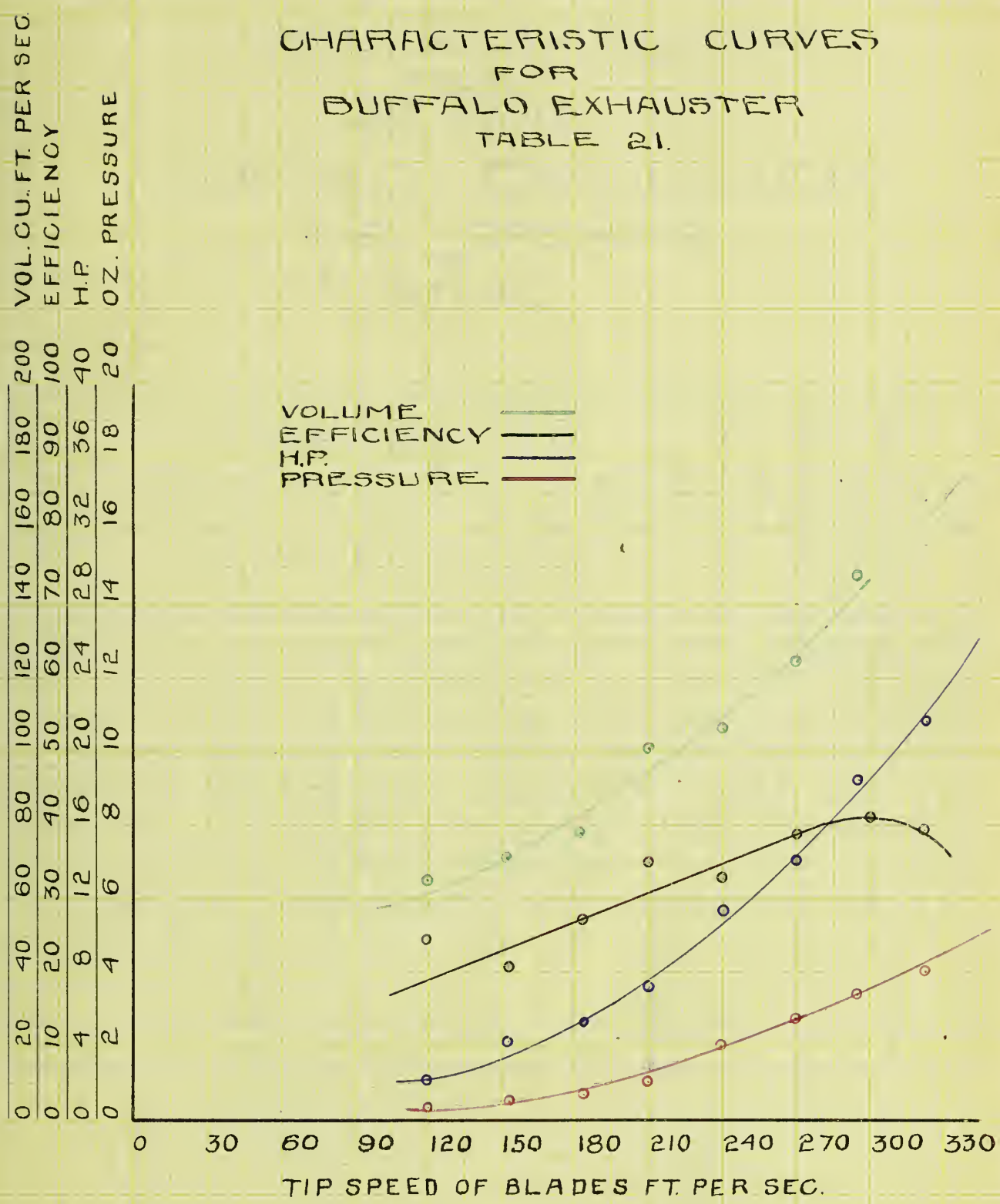
1902

1903

1904

1905

CHARACTERISTIC CURVES FOR BUFFALO EXHAUSTER TABLE 21.

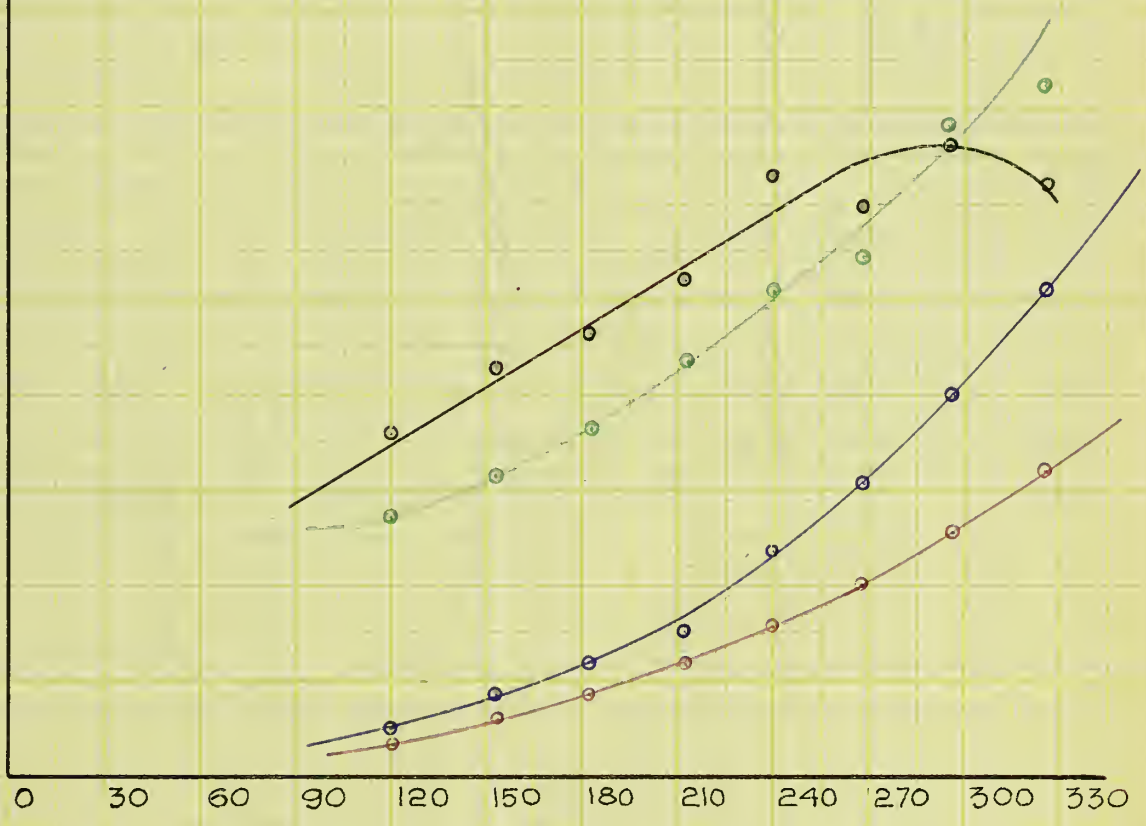


CHARACTERISTIC CURVES FOR BUFFALO EXHAUSTER TABLE 22.

VOL. CU. FT. PER. SEC.
EFFICIENCY
H.P.
OZ. PRESSURE

200	180	160	140	120	100	80	60	40	20	0
100	90	80	70	60	50	40	30	20	10	0
40	36	32	28	24	20	16	12	8	4	0
20	18	16	14	12	10	8	6	4	2	0

VOLUME
EFFICIENCY
H.P.
PRESSURE



TIP SPEED OF BLADES FT. PER SEC.

DATA AND RESULTS
FOR
40" INCH
BUFFALO EXHAUSTER
1/4 OF
INTAKE

[illegible]

CHARACTERISTIC CURVES FOR BUFFALO EXHAUSTER TABLE 23

VOL. CU. FT. PER SEC
EFFICIENCY
H.P.
OZ. PRESSURE

0	20	40	60	80	100	120	140	160	180	200
0	10	20	30	40	50	60	70	80	90	100
0	4	8	12	16	20	24	28	32	36	40
0	2	4	6	8	10	12	14	16	18	20

VOLUME
EFFICIENCY
H.P.
PRESSURE

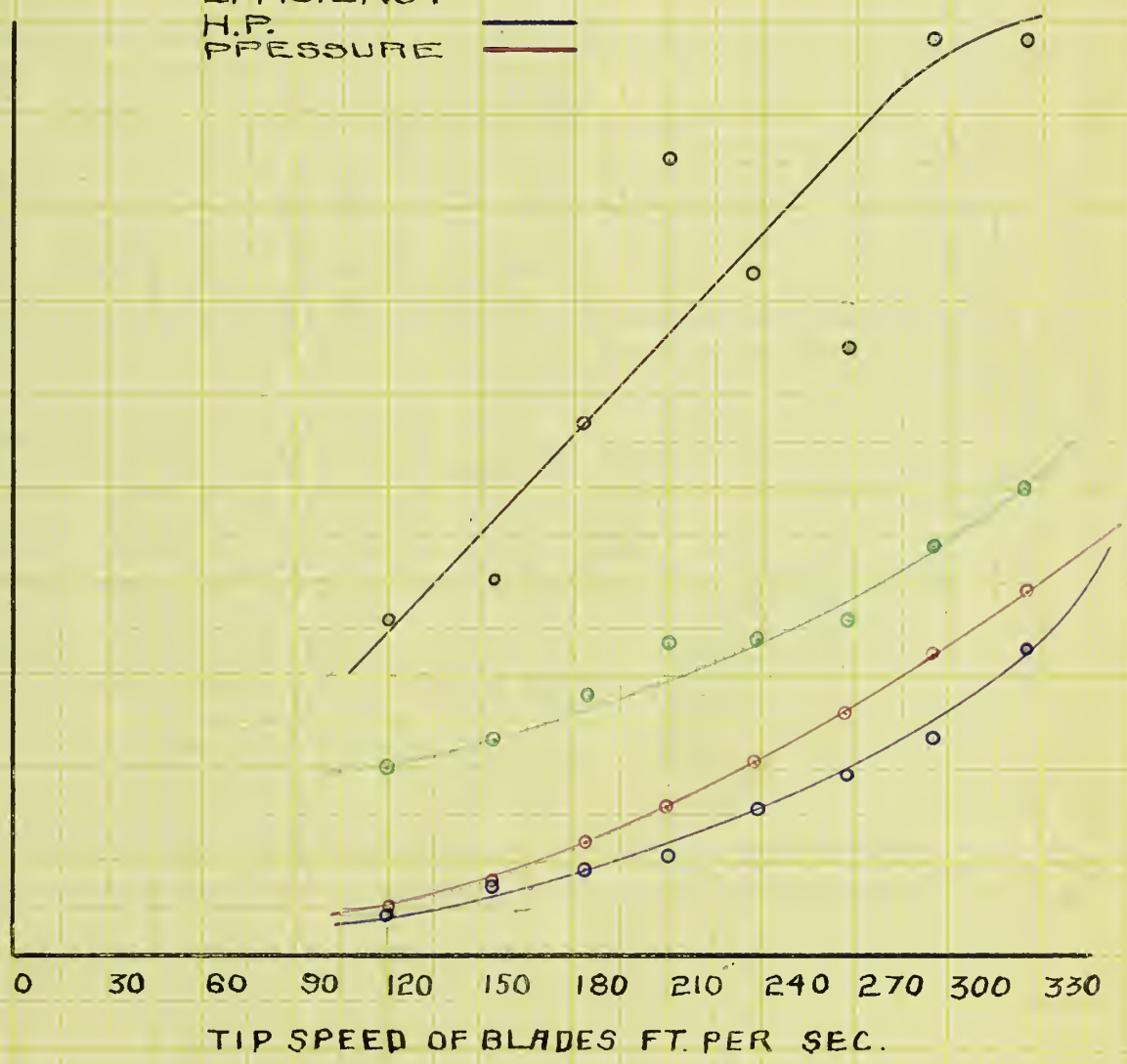




TABLE 24.

DATA AND RESULTS
FOR
40 INCH
BUFFALO EXHAUSTER
O OPENING
OF
INTAKE

[illegible]

CHARACTERISTIC CURVES FOR BUFFALO EXHAUSTER TABLE 24

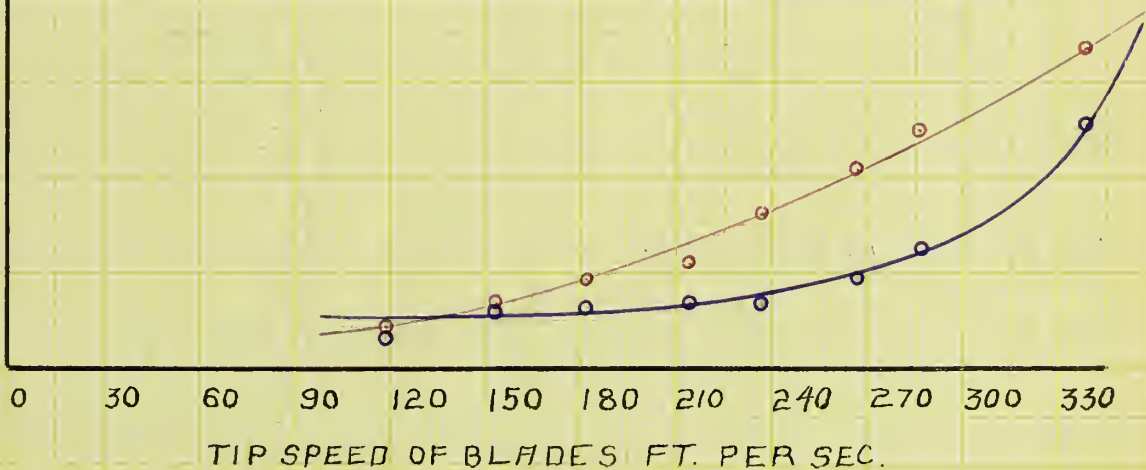
VOL. CU.FT. PER SEC
EFFICIENCY
H.P.
OZ. PRESSURE

200	180	160	140	120	100	80	60	40	20	0
100	90	80	70	60	50	40	30	20	10	0
40	36	32	28	24	20	16	12	8	4	0
20	18	16	14	12	10	8	6	4	2	0

VOLUME
EFFICIENCY
H.P.
PRESSURE

==

==



Results.

Tables and Curves:— The results of each experiment are included in a series of five tables, with the exception of the Stintvant Blower No. 1, which has only four, because it had only four openings or conditions of its discharge.

Characteristic curves, for each table of results, are plotted on the page following the table, for each fan.

Discussion of Results:—

Power Required by the Fan.— By study of the results, it will be found that the maximum power consumed is for the full discharge opening, when the pressure is the lowest, and that the pressure consumed varies

approximately as the square of the speed for each discharge opening. With a closed gate the power necessary to drive the fan is very small, notwithstanding the fact that the pressure is the highest. This is because there is no air passing through the fan.

Pressure:— The pressure is the lowest at the full discharge opening and becomes a maximum at the zero opening.

However, for three fourths gate opening the pressure recorded was very often as high as for a closed gate. For quarter opening of the discharge the pressure does not increase so fast in relation to the speed,

as did the H.P. required to drive the fan, while for half opening of the discharge their ratios of increase were about equal. With the three quarter and closed discharge the pressure increased about as the cube of the speed.

Velocity:— In all cases the velocity increased about as the cube of the speed.

Efficiency:— The efficiency is always the lowest for the full gate opening, when the discharge is a maximum. This is due to the fact that the air is discharged at a very low pressure as compared to the other gate openings. The

efficiency increases approximately, directly as the speed and as the size of the discharge opening decreases, up to a certain point, which varies in different fans, and then falls quickly to zero, as the gate is closed.





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